



Tallinn University of Technology, May 2025

**TAL
TECH**

Estonian Doctoral School



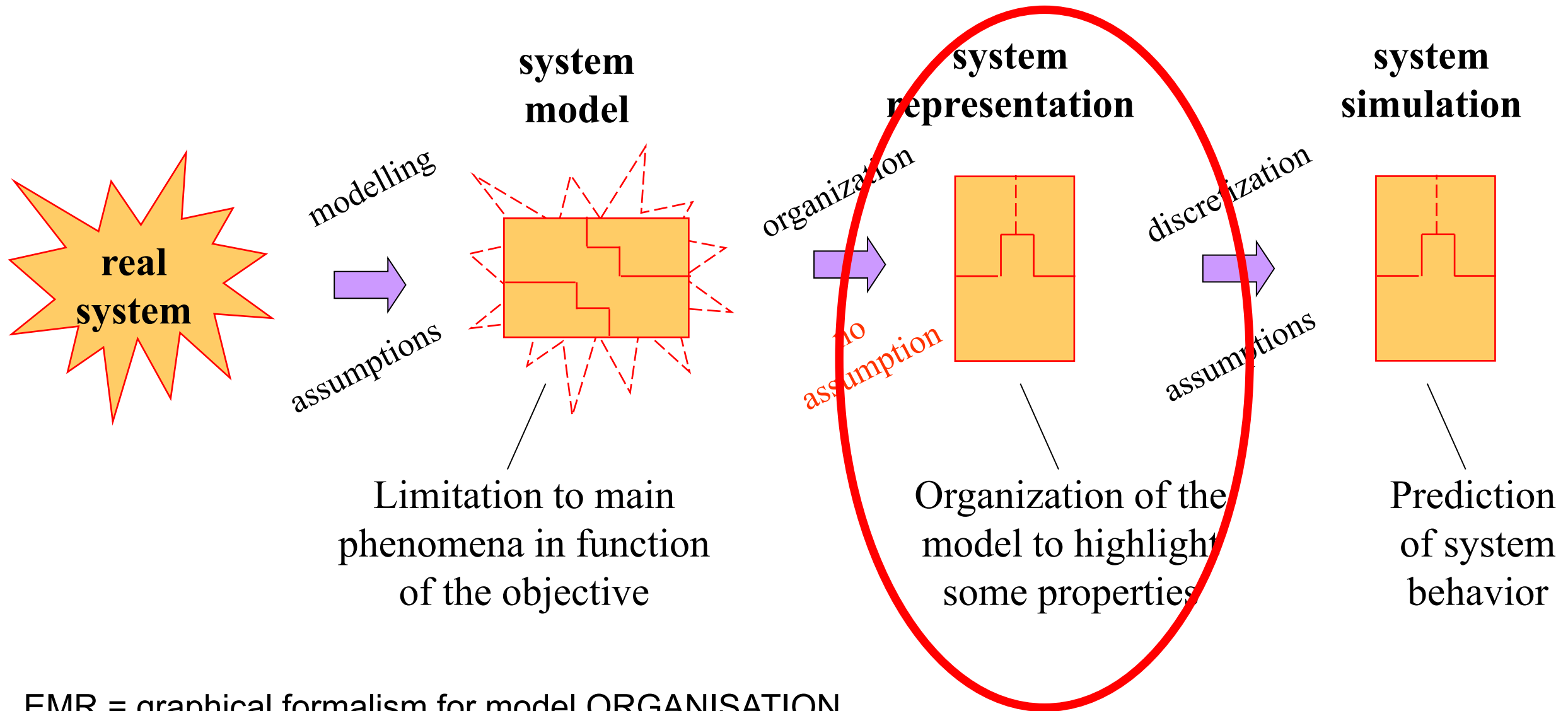
“Energetic Macroscopic Representation”

.....

Prof. Betty LEMAIRE-SEMAIL, Prof. Alain BOUSCAYROL,

Based on the EMR summer school
and Master “Electrical Engineering for
sustainable development” course at Univ. Lille



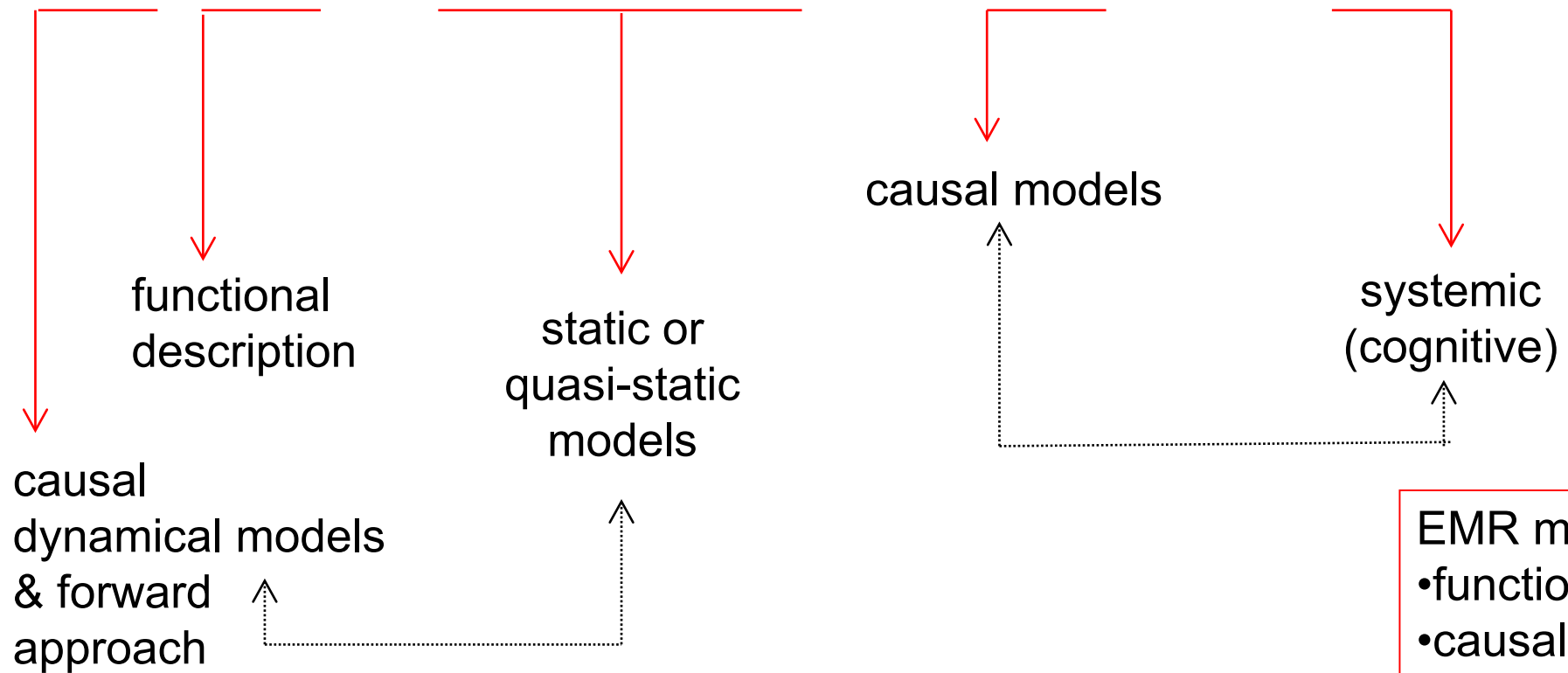


EMR = graphical formalism for model ORGANISATION
(after the modelling step)

A graphical description is chosen depending on objectives

EMR objective:

- real-time control and energy management of energy conversion systems



EMR must be

- functional
- causal
- systemic

-  **EMR elements**
-  **Association rules**
-  **EMR of a complete system**
-  **Example**

1

EMR elements

2

Association rules

3

EMR of a complete system

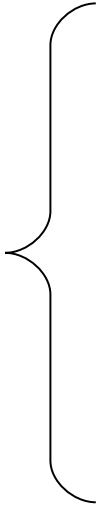
4

Example

Key aspects for energy conversion systems:

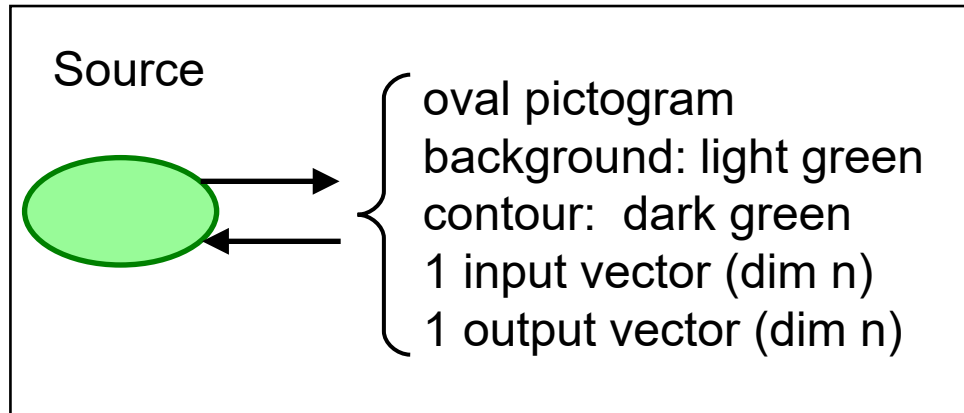
- Causality principle (energy)
- Interaction principle (Systemics)

Only 4 energy functions
are required to describe
energy conversion systems



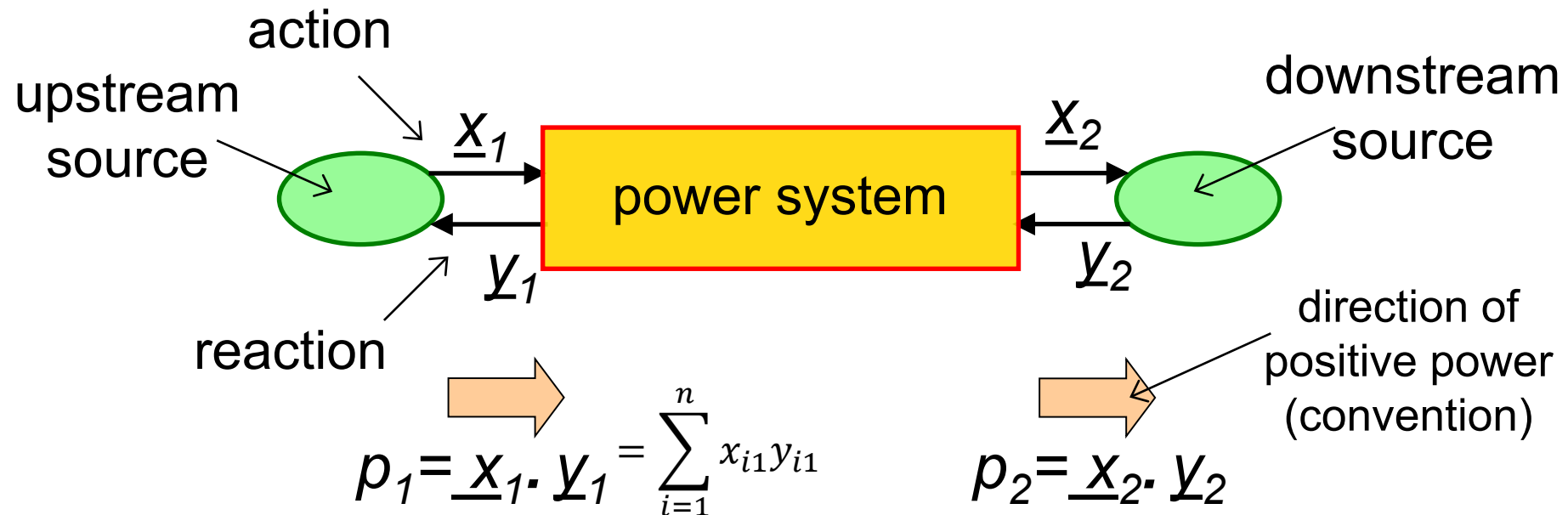
Energy sources
Energy storage
Energy conversion
Energy distribution

EMR = 4 graphical elements associated with the 4 energy functions

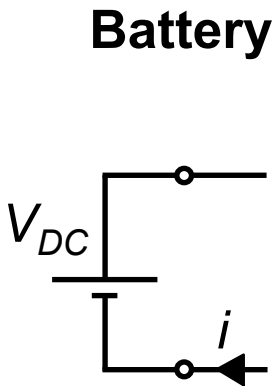


terminal elements which represent the environment of the studied system

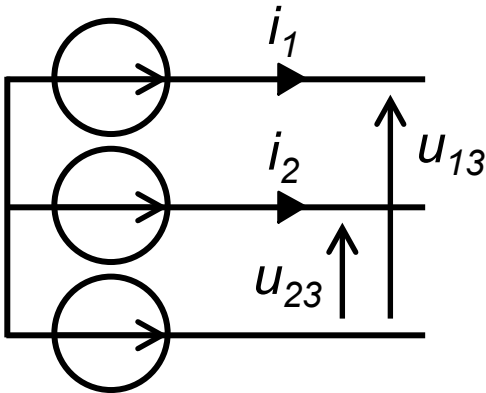
generator and/or receptor of energy



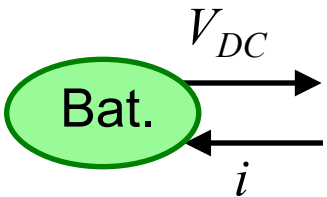
structural
description

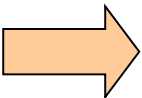


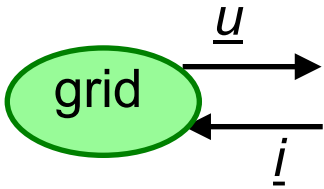
Electrical grid

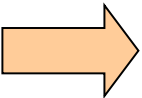


EMR
(functional
description)




 $p(t) = V_{DC}(t) i(t)$

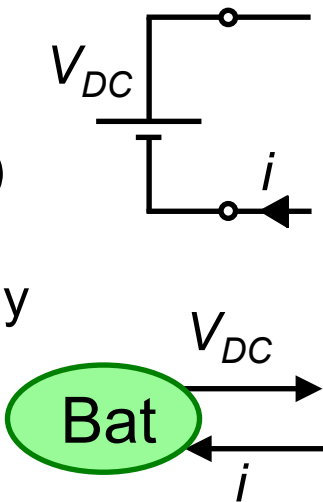



 $p(t) = \underline{u}(t) \underline{i}(t) = u_{13}(t) i_1(t) + u_{23}(t) i_2(t)$

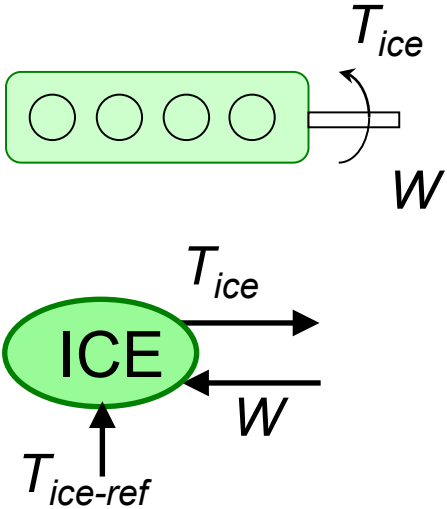
$$\underline{u} = \begin{bmatrix} u_{13} \\ u_{23} \end{bmatrix} \quad \underline{i} = \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$$

2 independent currents!
2 independent voltages!

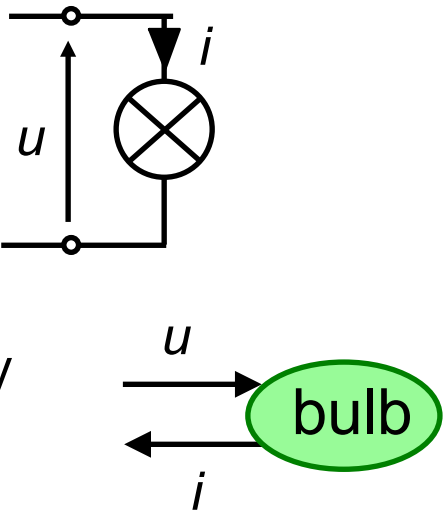
Battery
(voltage source)
generator and
receptor of energy



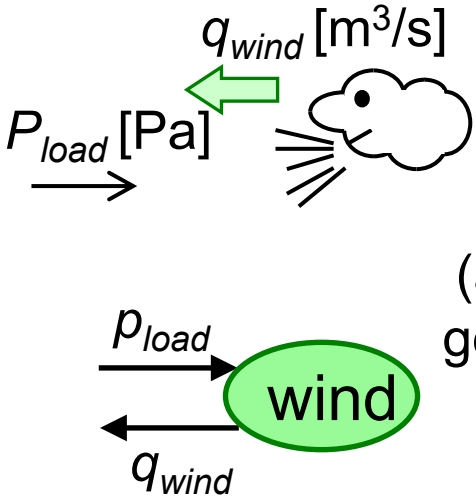
IC engine
(torque source)
generator
of energy

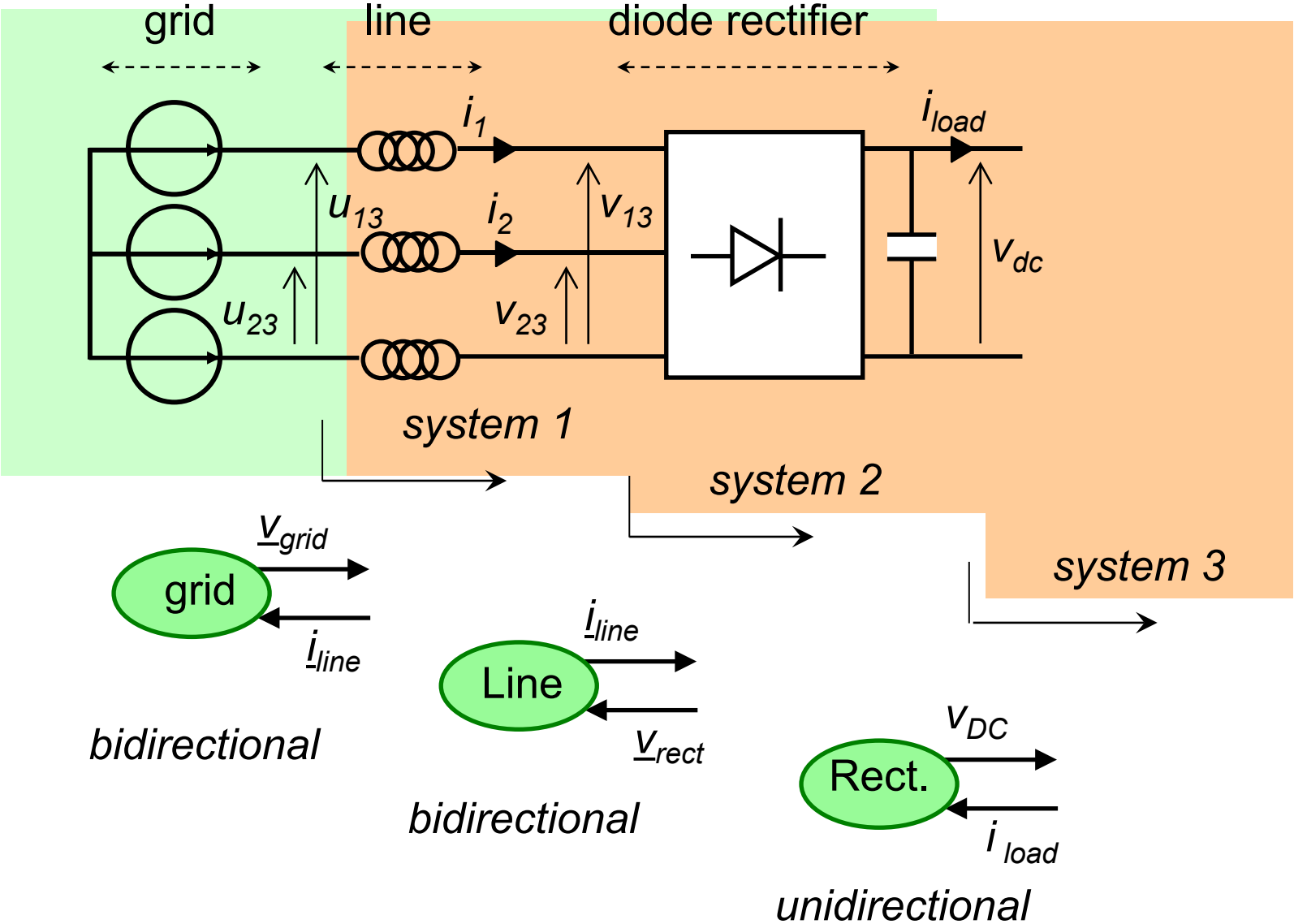


Ligthing bulb
receptor of energy

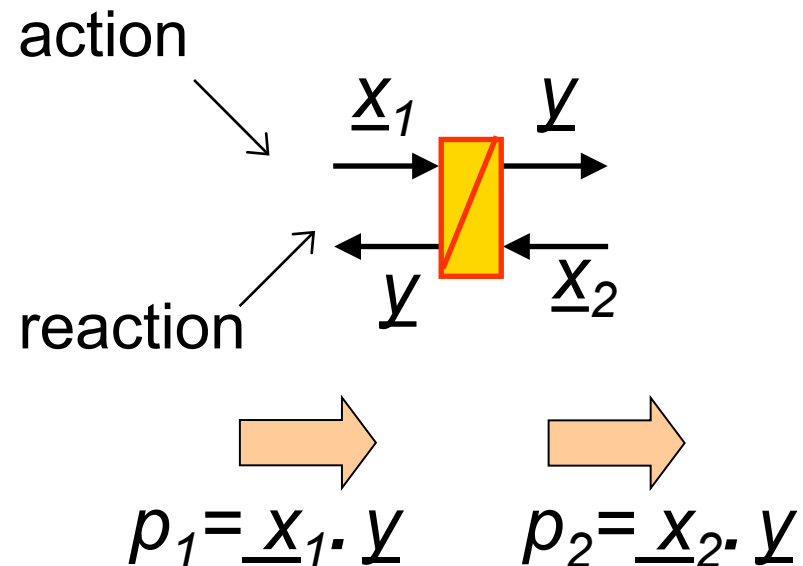
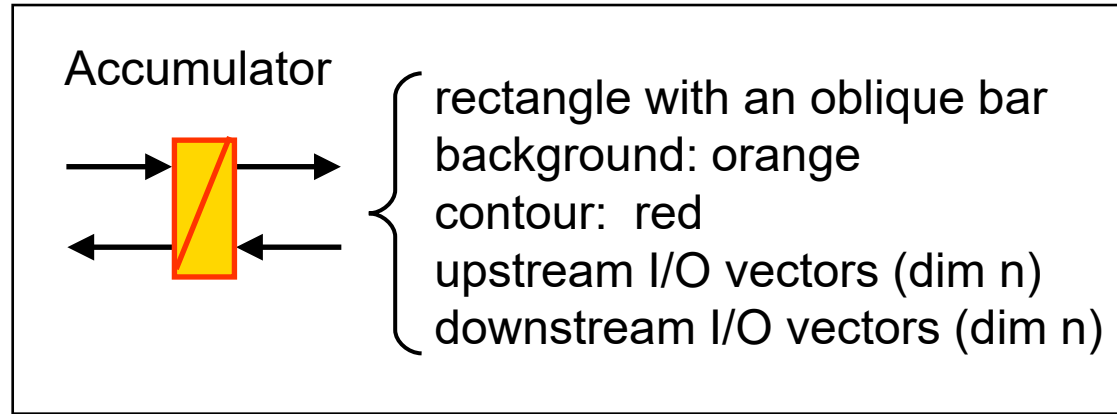


Wind
(air flow source)
generator energy





Border of the system?



internal accumulation of energy (with or without losses)

causality principle

Output variable = Energetic variable

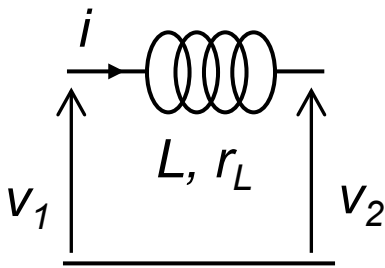
$$\text{output}(s) = \int \text{input}(s)$$

$$\underline{y} \propto \int f(\underline{x}_1, \underline{x}_2) dt$$

$\underline{y}$ = output, delayed with regard to input changes

fixed I/O (causal description)

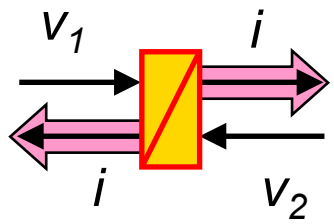
structural description



functional mathematical Model

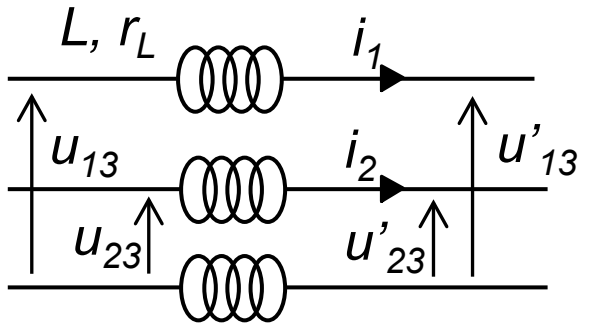
$$L \frac{d}{dt} i + r_L i = v_1 - v_2$$

EMR (causal functional representation)

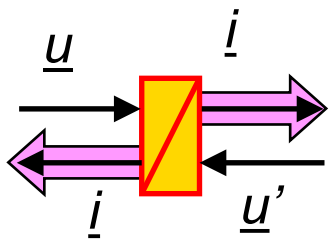

$$i = \frac{1}{L} \int_0^t (v_1 - v_2 - ri) dt$$

output = integral function of inputs
output delayed from inputs

3-phase line

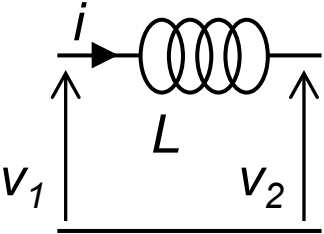


$$[L] \frac{d}{dt} \underline{i} + r_L \underline{i} = \frac{1}{3} \begin{bmatrix} 2 & -1 \\ -1 & 2 \end{bmatrix} (\underline{u} - \underline{u}')$$

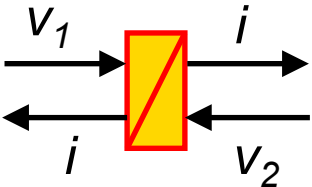


output = current vector (dimension 2)

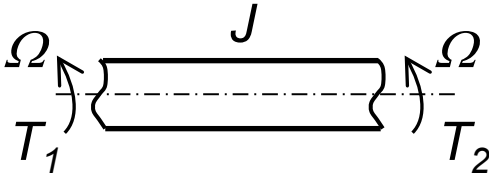
inductor



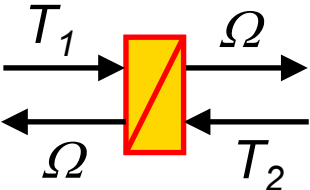
$$E = \frac{1}{2} Li^2$$



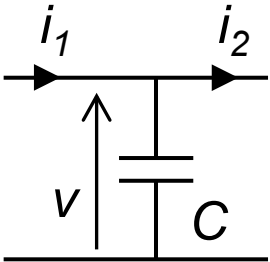
inertia



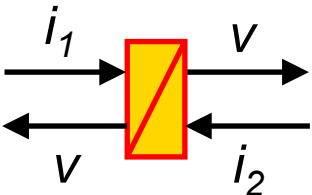
$$E = \frac{1}{2} J \Omega^2$$



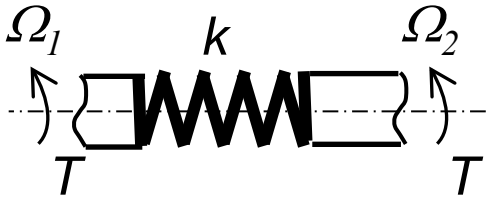
capacitor



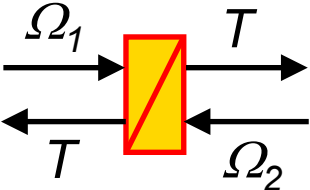
$$E = \frac{1}{2} C v^2$$

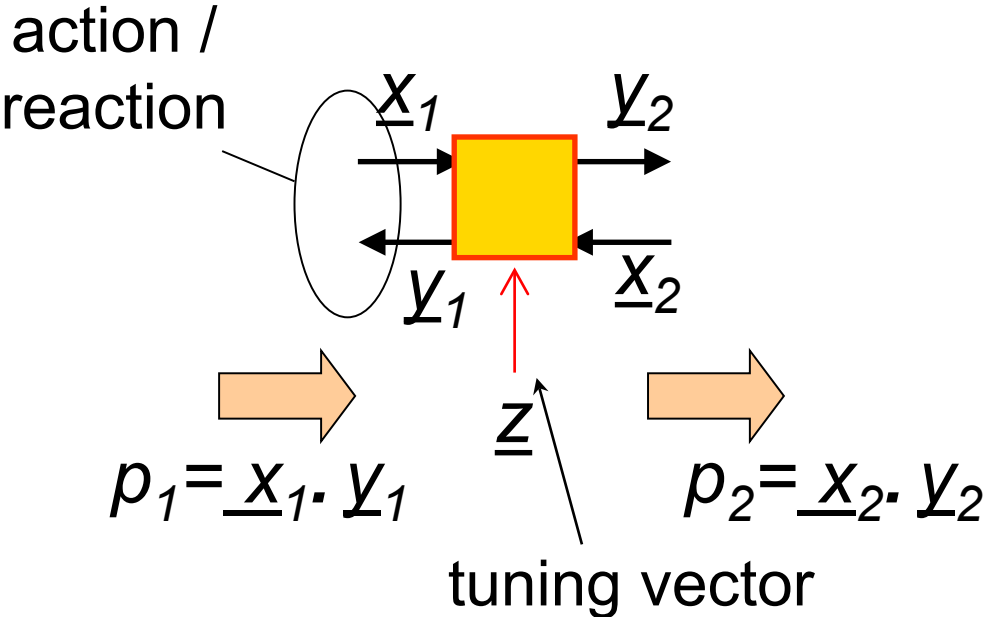
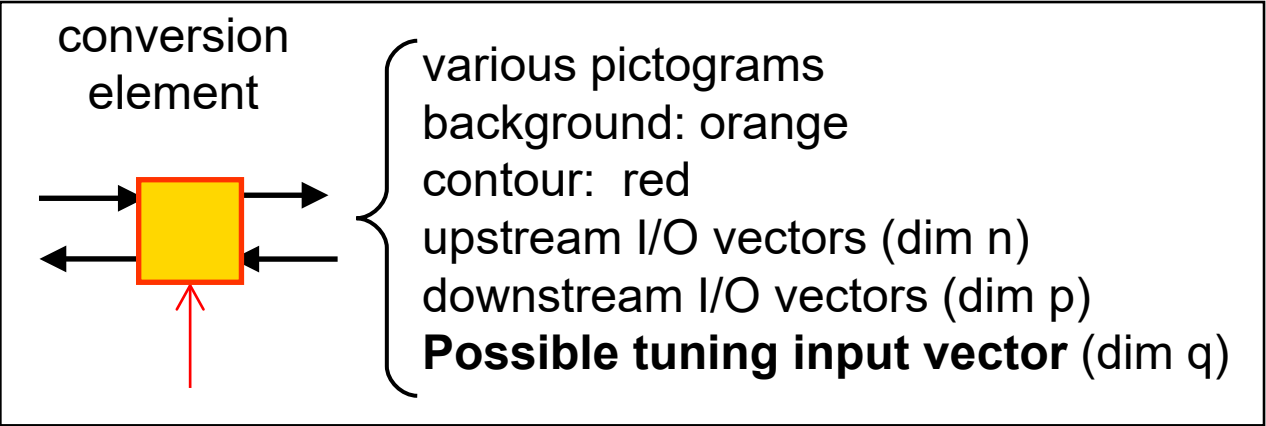


stiffness



$$E = \frac{1}{2} \frac{1}{k} T^2$$



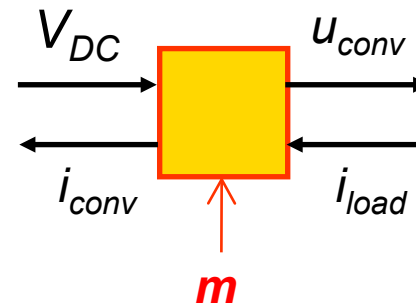
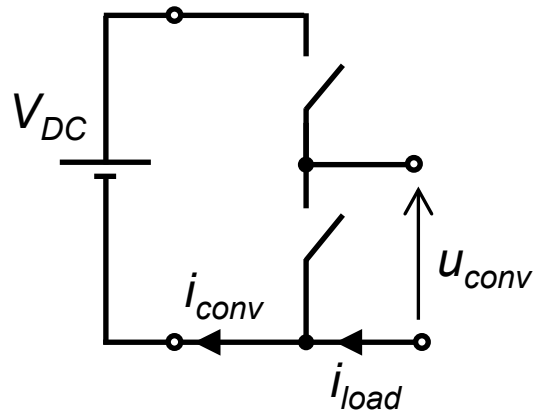
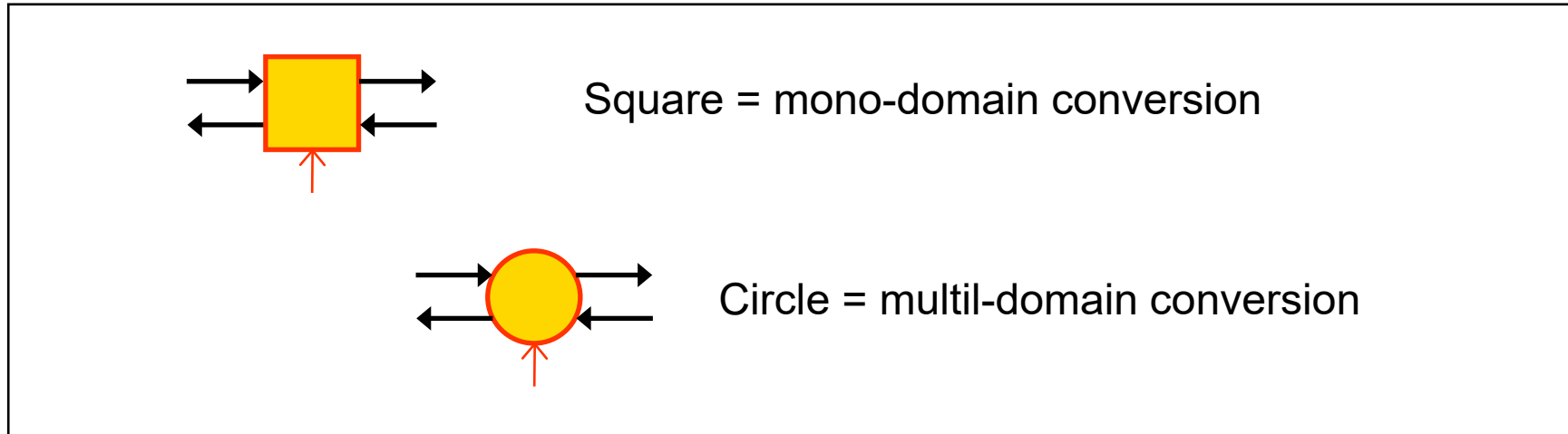


**conversion of energy
without energy
accumulation**
(with or without
losses)

$$\begin{cases} \underline{y}_2 = f(\underline{x}_1, \underline{z}) \\ \underline{y}_1 = f(\underline{x}_2, \underline{z}) \end{cases}$$

no delay! ←

↓
upstream and downstream
I/O can be permuted
(floating I/O)

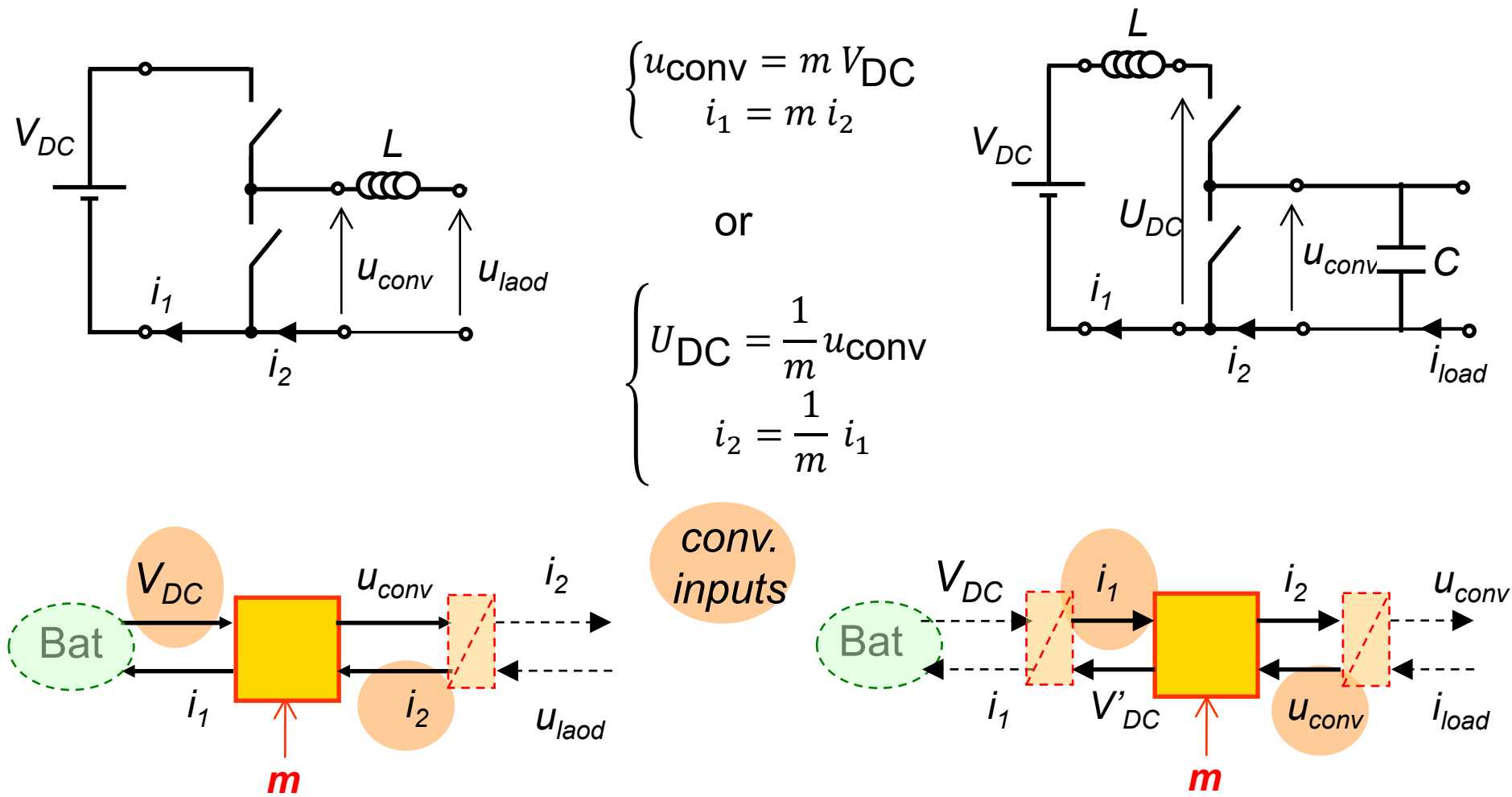


$$\begin{cases} u_{conv} = m V_{DC} \\ i_{conv} = m i_{load} \end{cases}$$

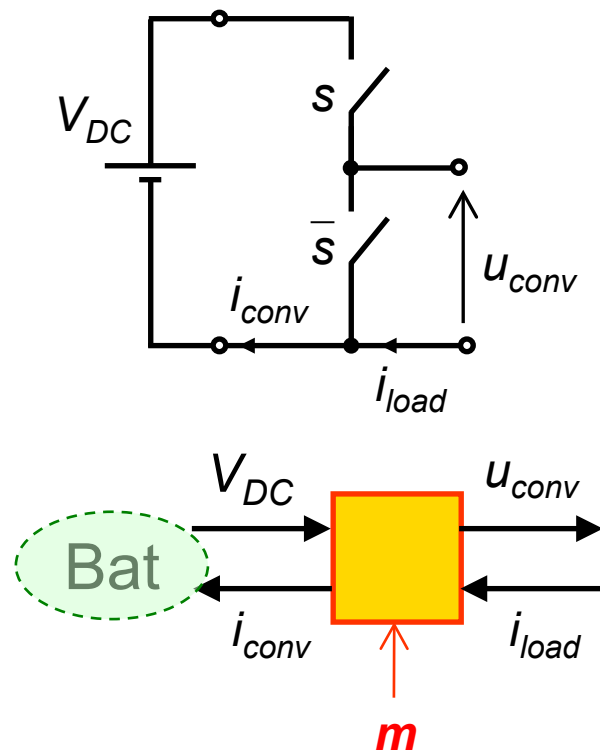
m : modulation function of the converter

$$\langle m \rangle = D$$

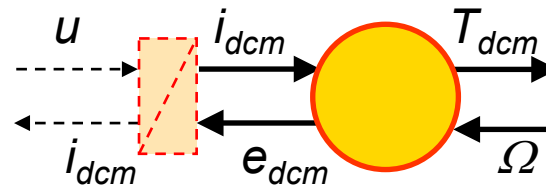
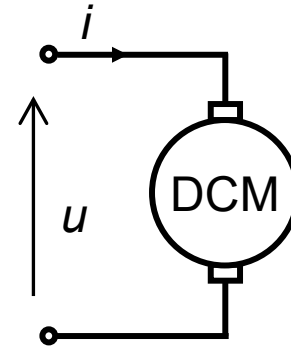
= duty cycle



I/O are defined by accumulation elements

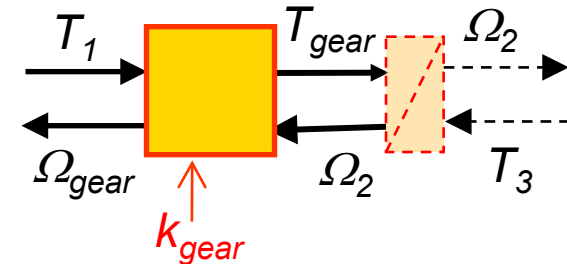
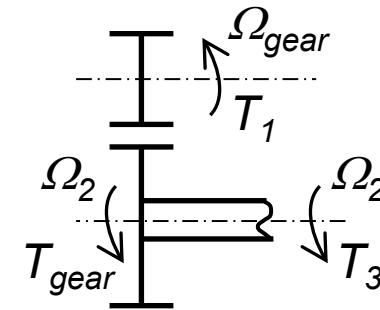


$$\begin{cases} u_{conv} = m V_{DC} \\ i_{conv} = m i_{load} \end{cases}$$



$$\begin{aligned} L \frac{d}{dt} i_{dcm} + r i_{dcm} \\ = u - e_{dcm} \end{aligned}$$

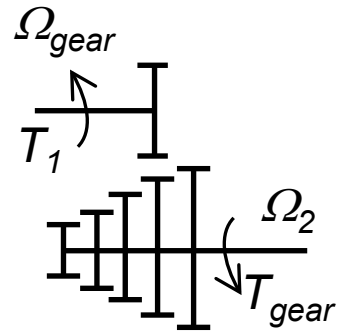
$$\begin{cases} T_{dcm} = k_{\phi} i_{dcm} \\ e_{dcm} = k_{\phi} \Omega \end{cases}$$



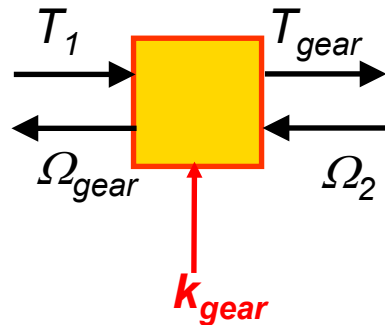
$$\begin{cases} T_{gear} = k_{gear} T_1 \\ \Omega_{gear} = k_{gear} \Omega_2 \end{cases}$$

$$J \frac{d}{dt} \Omega_2 = T_{gear} - T_3$$

5-speed gearbox

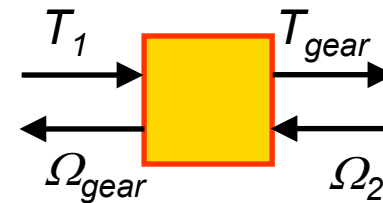
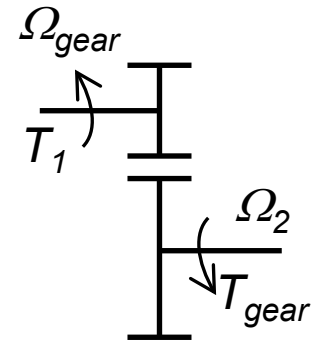


$$\begin{cases} T_{\text{gear}} = k_{\text{gear}} T_1 \\ \Omega_{\text{gear}} = k_{\text{gear}} \Omega_2 \end{cases}$$



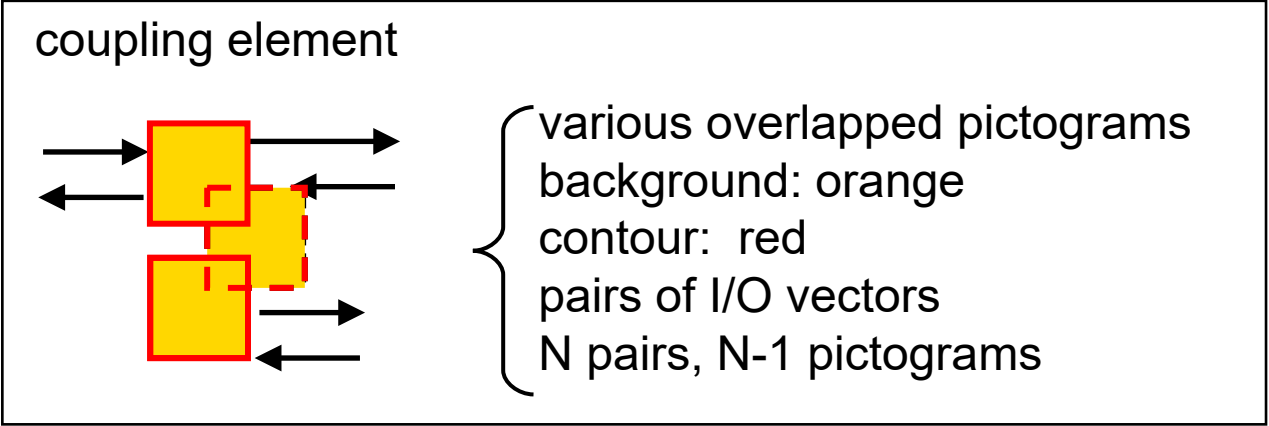
$$k_{\text{gear}} \in \{k_1, k_2, k_3, k_4, k_5\}$$

fixed gear

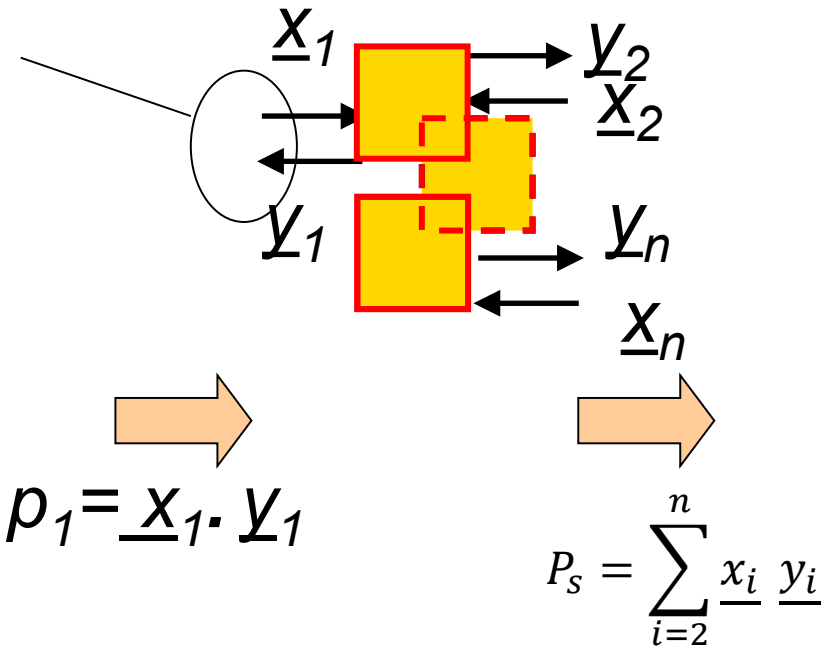


(no tuning input)

$$k_{\text{gear}} = \text{constant}$$



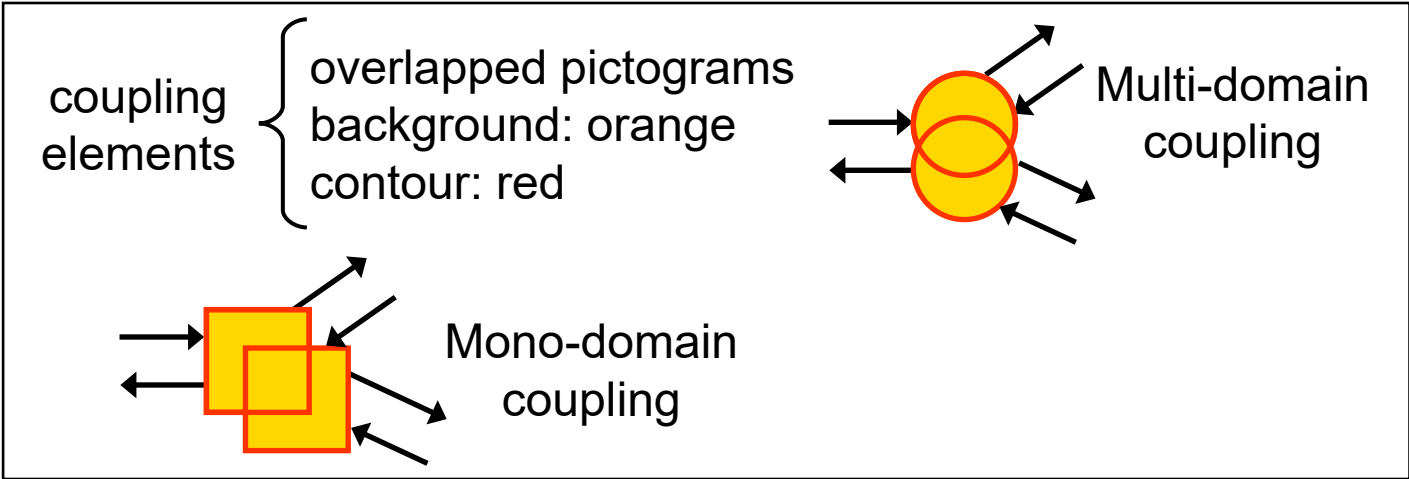
action /
reaction



distribution of energy
without energy
accumulation
without tuning
(with or without losses)

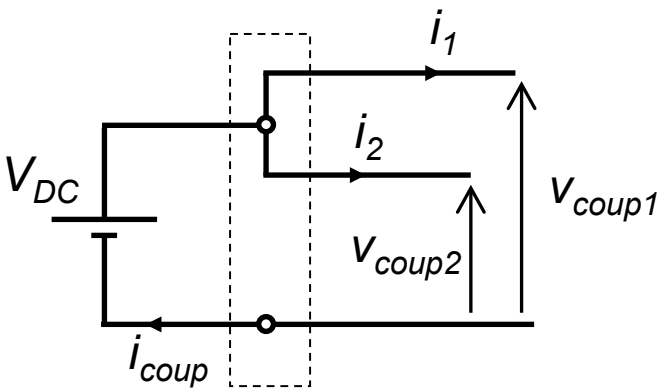
$\begin{cases} \underline{y}_1 = f_1(\underline{x}_1, \dots, \underline{x}_n) \\ \underline{y}_n = f_n(\underline{x}_1, \dots, \underline{x}_n) \end{cases}$ no delay!

N elements connected
(N-1) overlapped pictograms

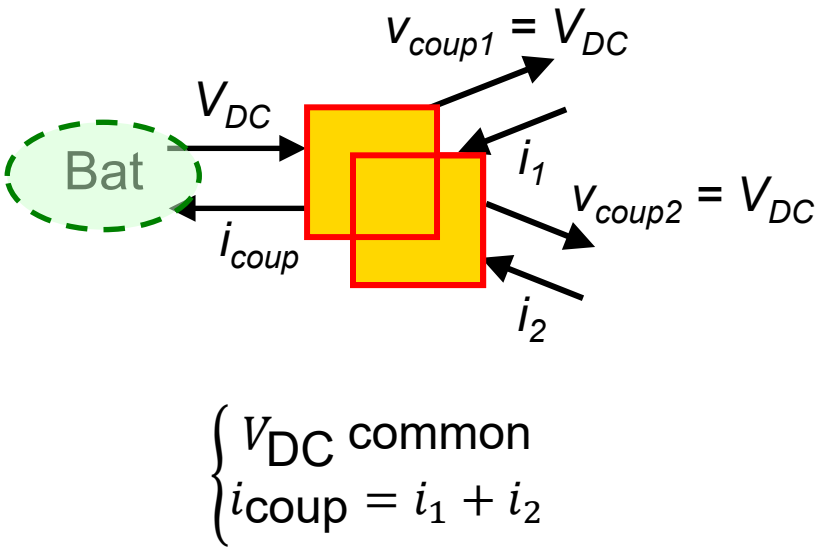


distribution
of energy

no tuning
vector



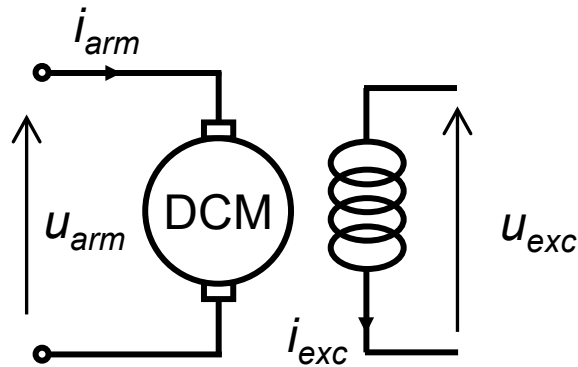
parallel connexion



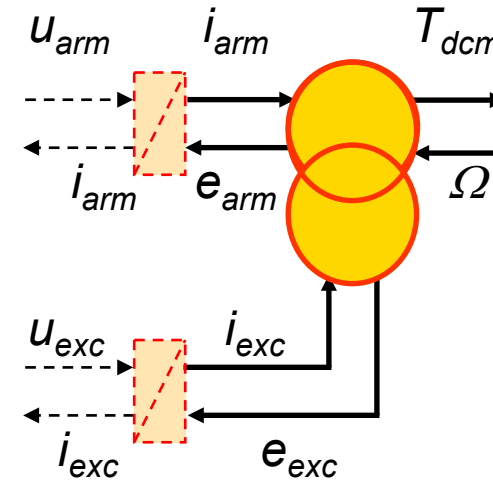
3 electrical elements
Connected
(battery, load 1, load 2)

2 overlapped
orange squares

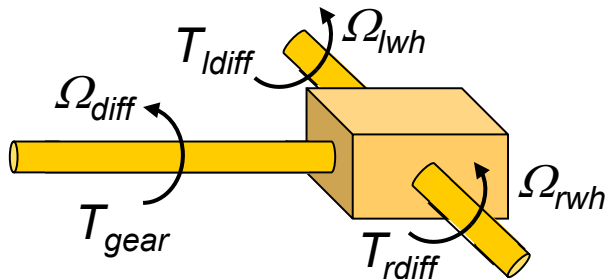
Field winding DC machine



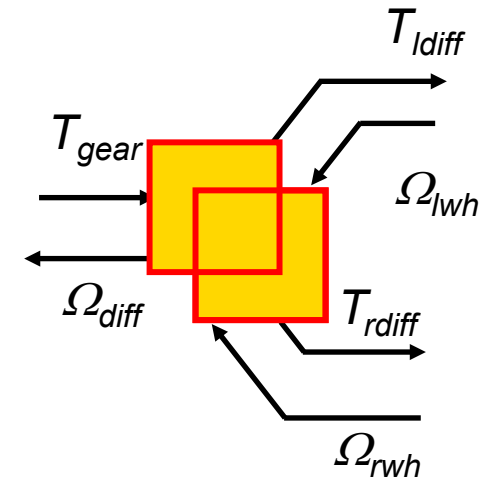
$$\begin{cases} T_{dcm} = k i_{exc} i_{arm} \\ e_{arm} = k i_{exc} \Omega \end{cases}$$

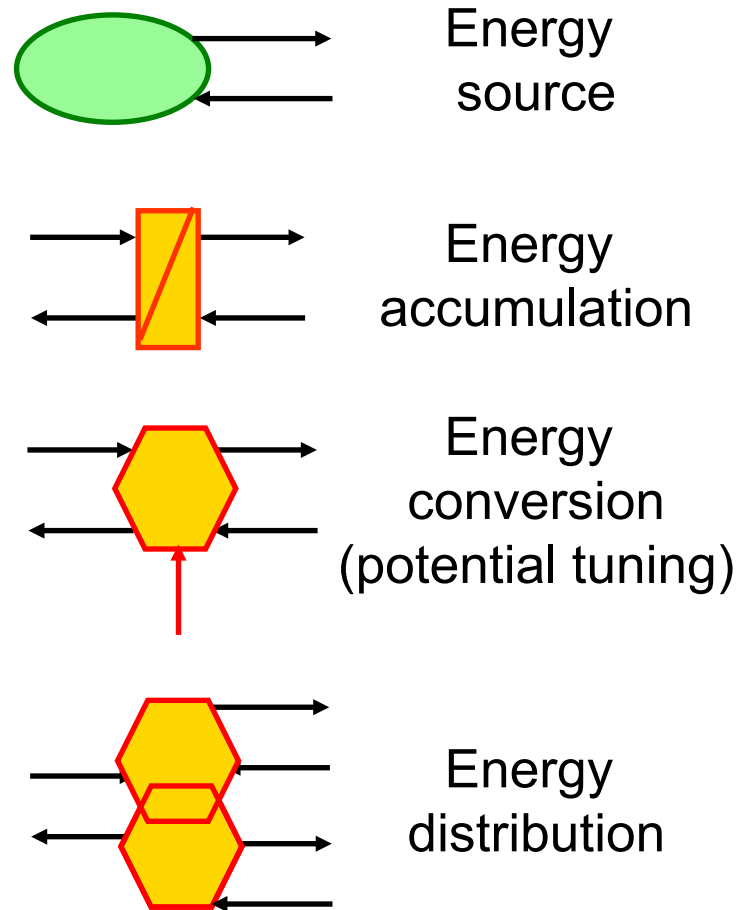


Mechanical differential



$$\begin{cases} T_{ldif} = T_{rdif} = \frac{T_{gear}}{2} \\ \Omega_{diff} = \frac{\Omega_{lwh} + \Omega_{rwh}}{2} \end{cases}$$

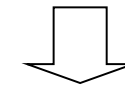




all elements connected
by action/ reaction (Systemics)

all power I/O defined
by accumulation elements
(causality)

only conversion elements
can have tuning inputs



valuable for control design

1

EMR elements

2

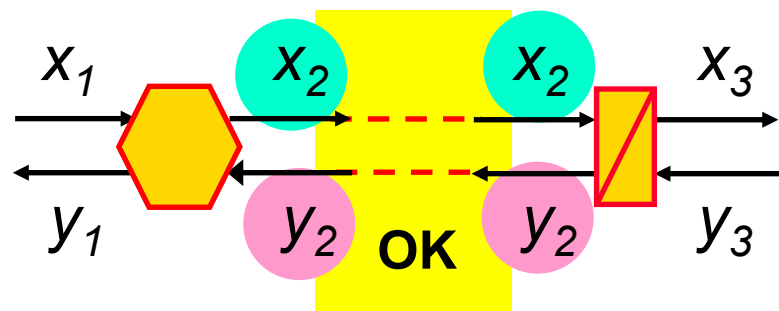
Association rules

3

EMR of a complete system

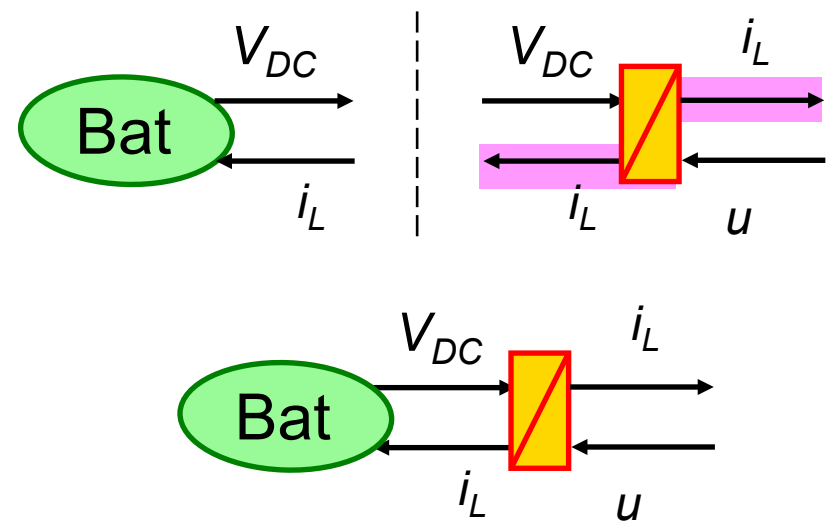
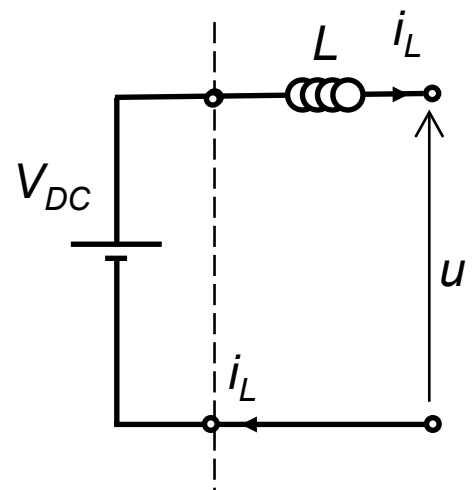
4

Example



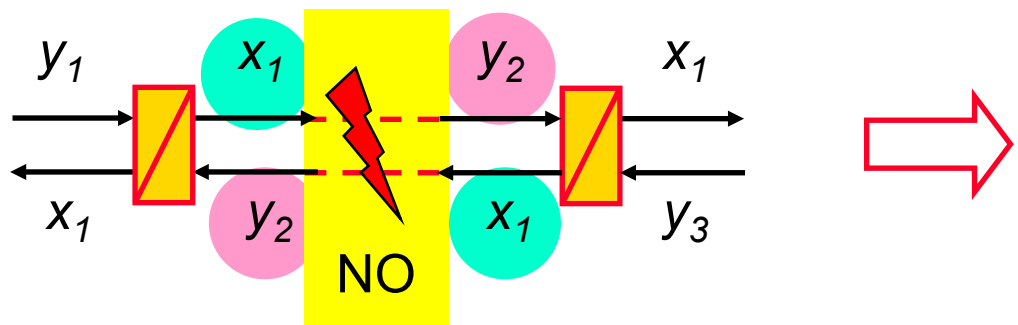
S1 and S2 any sub-systems

Example

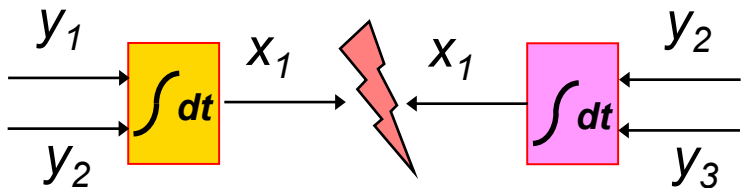


$$L \frac{d}{dt} i_L = V_{DC} - u$$

i energetic variable

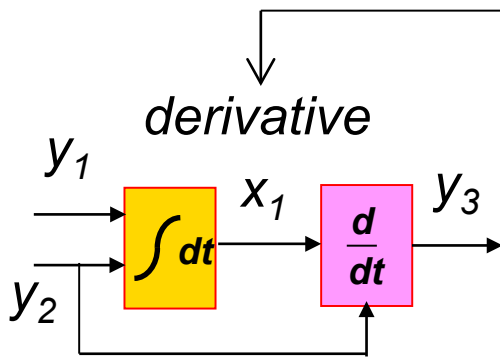


2 accumulation elements
impose the same
state variable x_1

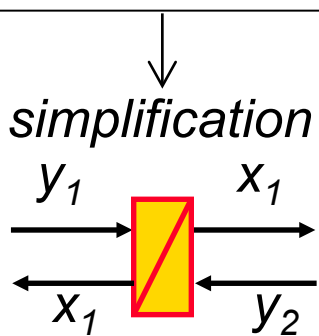


Conflict of association

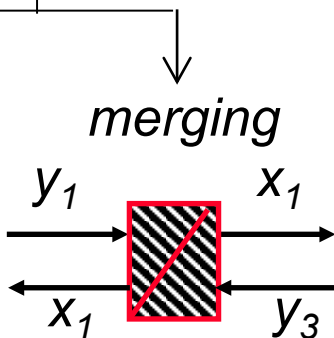
solutions



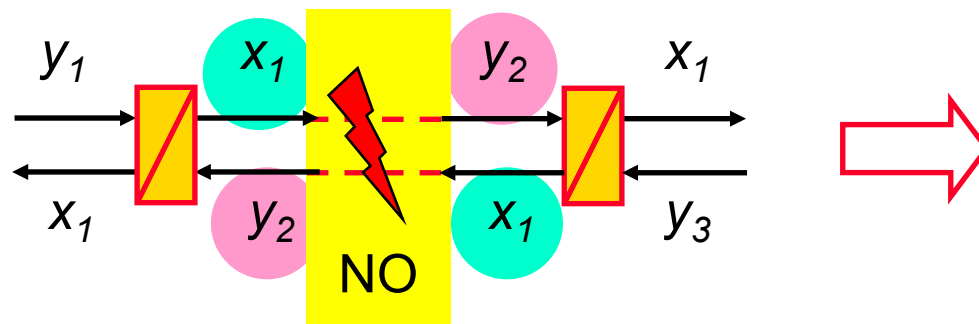
Structural / mathematical
solution / non physical



Cartesian approach
/ non physical



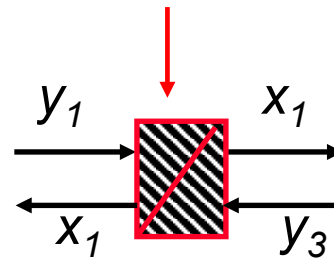
1 equivalent function for
2 elements / systemic



2 accumulation elements
would impose the same
state variable x_1

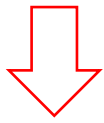
Conflict of association

merging



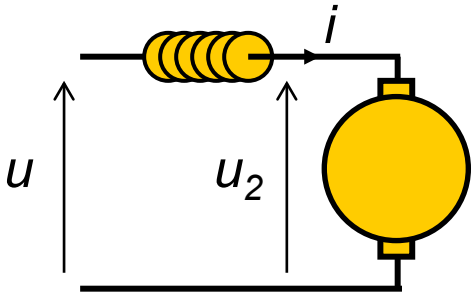
1 equivalent function for
2 elements / systemic

EMR only for detection of
conflict of association



come back on modelling
for mathematical solving

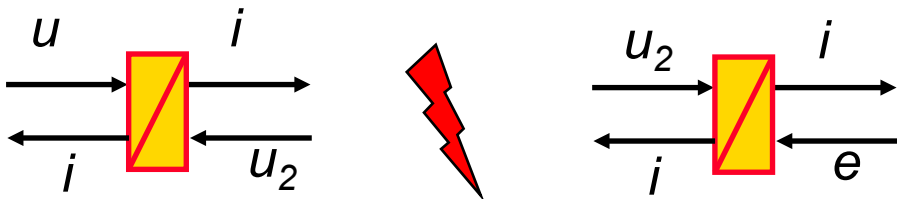
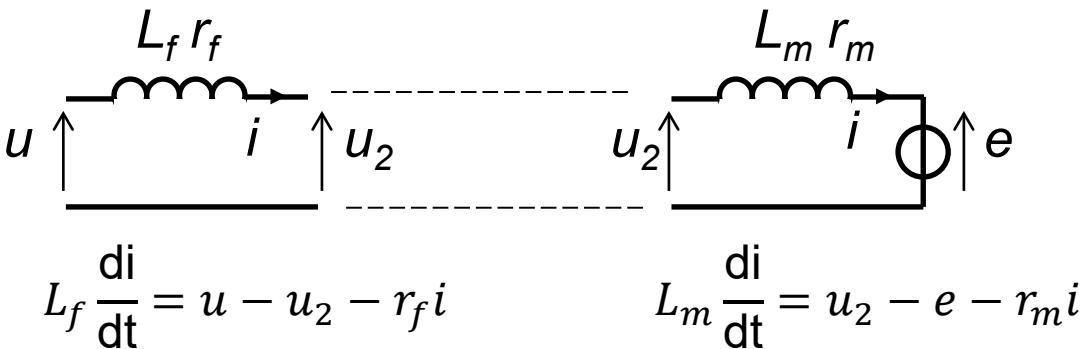
DC machine and smoothing inductor



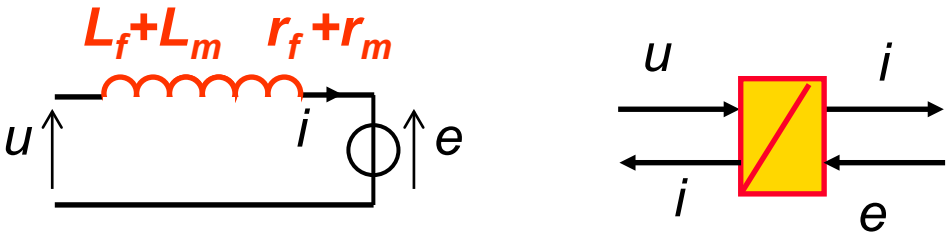
Assumption: L_f, L_m constant

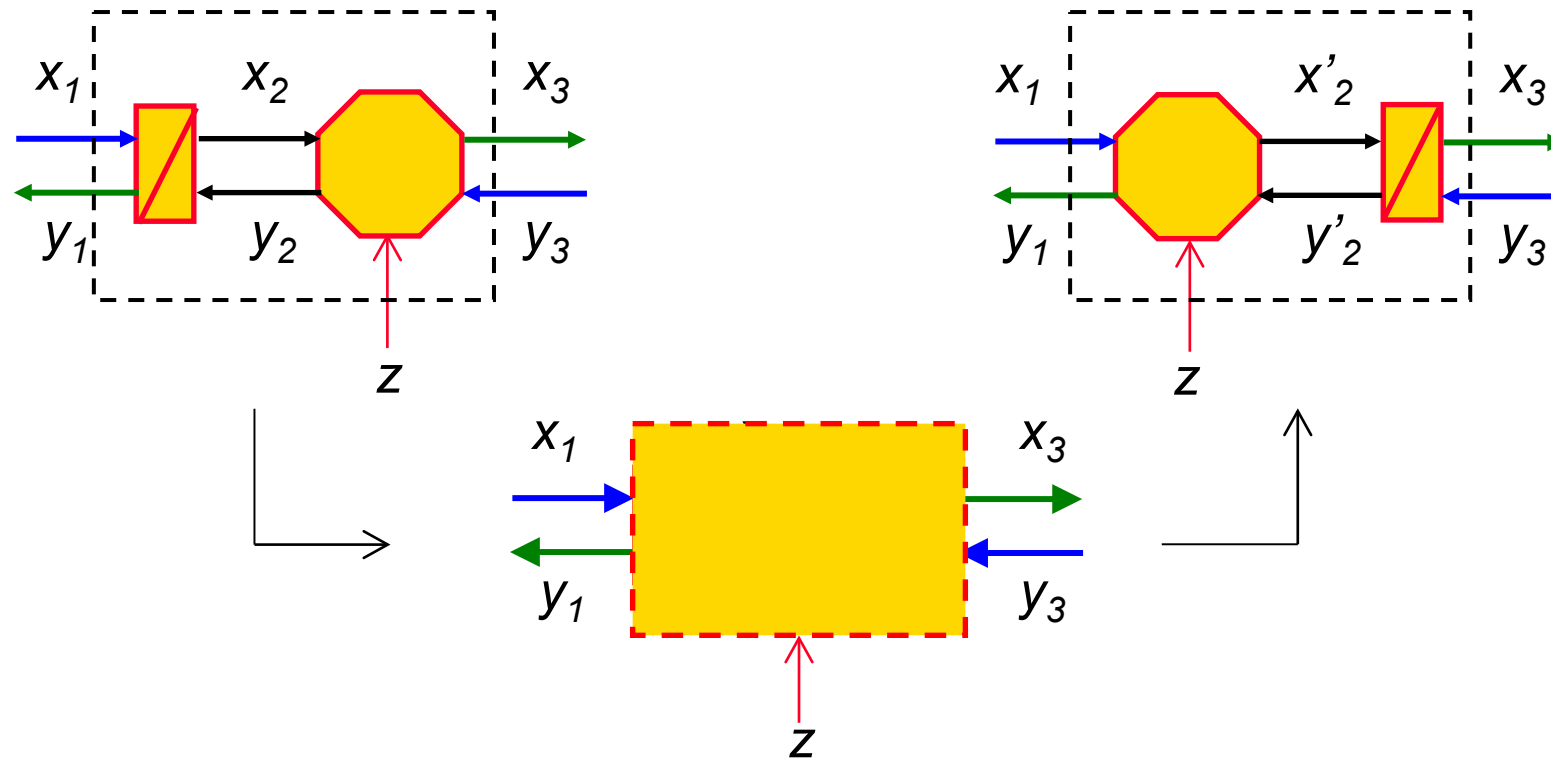
Remark:

$\frac{L_f + L_m}{r_f + r_m}$	$\frac{L_f}{r_f} + \frac{L_m}{r_m}$	$\frac{L_f}{r_f}$
↓	↓	↓
merging (systemic)	Structural (Cartesian)	simplification

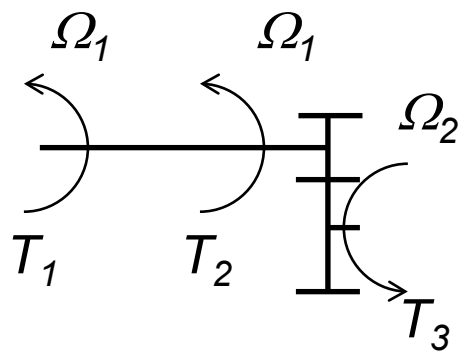


$(L_f + L_m) \frac{di}{dt} = u - e - (r_f + r_m) i$



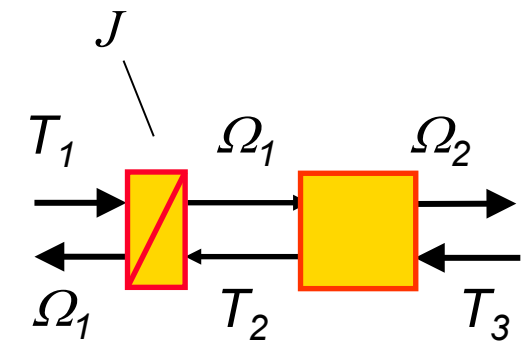


permutation possible if same global behavior:
 strictly the same effects (y_1 and x_3) from the same causes (x_1, y_3 and z)



$$J \frac{d}{dt} \Omega_1 = T_1 - T_2$$

$$\begin{cases} T_2 = k T_3 \\ \Omega_2 = k \Omega_1 \end{cases}$$



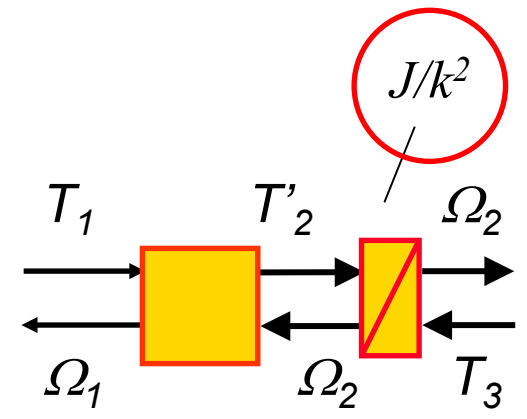
Shaft + gearbox

variable change

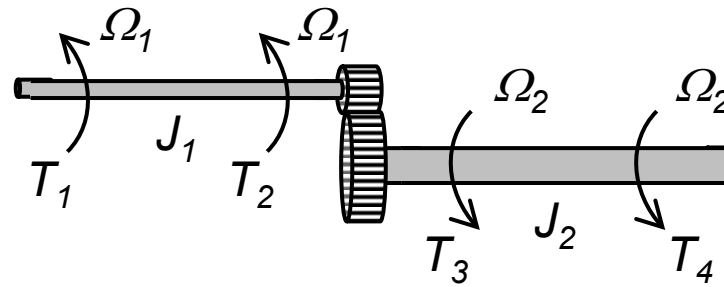
$$\frac{J}{k^2} \frac{d}{dt} \Omega_2 = T'_2 - T_3$$

no assumption
strict equivalence
(same model)

$$\begin{cases} T_2 = \frac{1}{k} T_1 \\ \Omega_1 = \frac{1}{k} \Omega_2 \end{cases}$$



Example: two inertia linked by a fix ratio gearbox



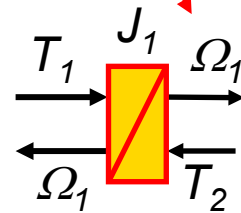
Models

$$J_1 \frac{d\Omega_1}{dt} = T_1 - T_2$$

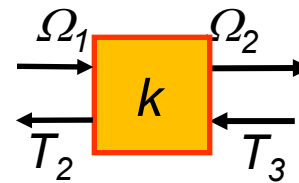
$$\begin{cases} \Omega_2 = K \cdot \Omega_1 \\ T_2 = K \cdot T_3 \end{cases}$$

$$J_2 \frac{d\Omega_2}{dt} = T_3 - T_4$$

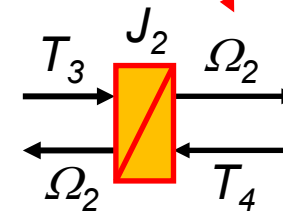
Representation



causal

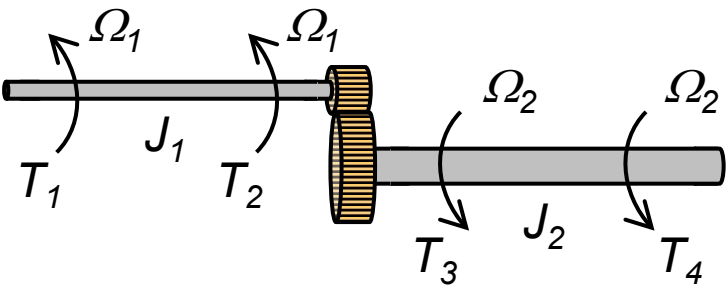


acausal



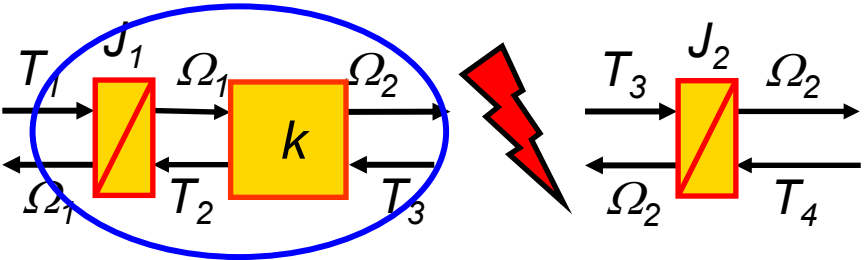
causal

Assumptions:
 J_1, J_2 constant
no backlash

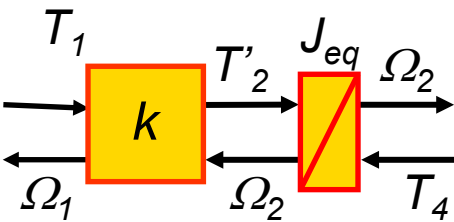
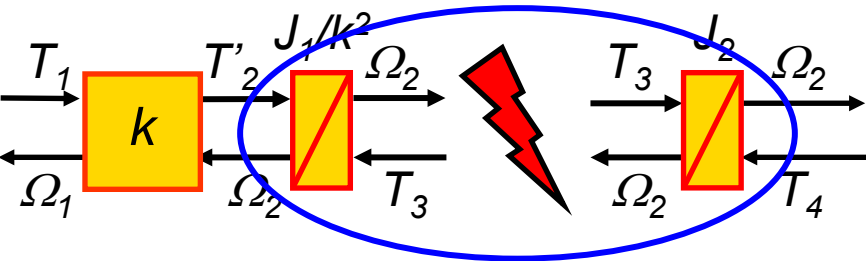


to solve conflict
of association

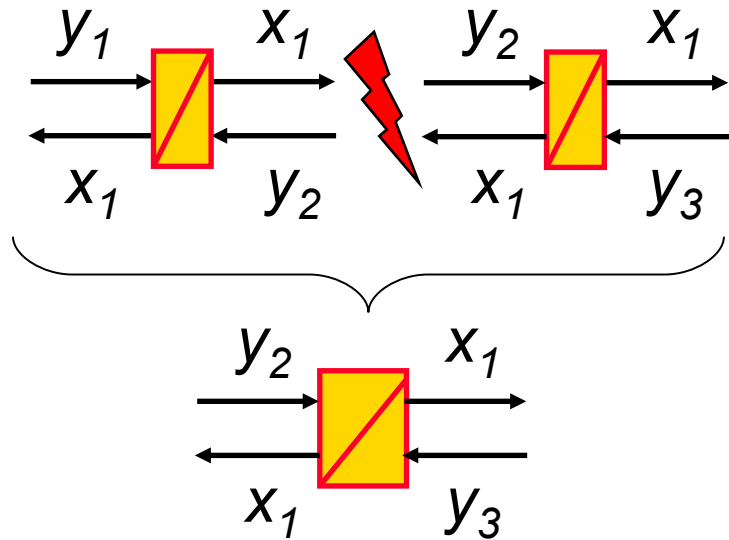
permutation



merging



$$J_{eq} = \frac{J_1}{k^2} + J_2$$



Priority to the function
by keeping the physical causality

Principle of holism
(systemic)

Main difference between structural and functional descriptions:

1 physical device: maybe 2 functions (e.g. two EMR elements)

Association of several physical devices: maybe a unique function (1 EMR element)

1

EMR elements

2

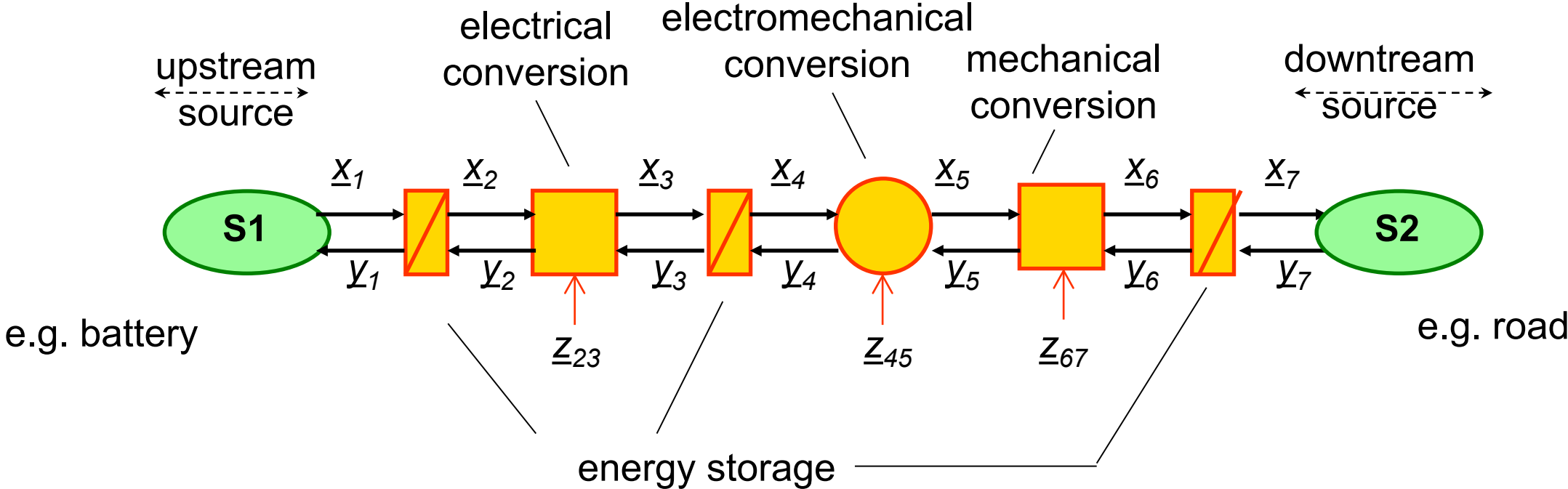
Association rules

3

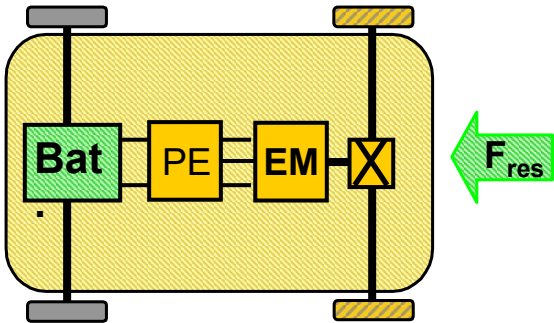
EMR of a complete system

4

Example



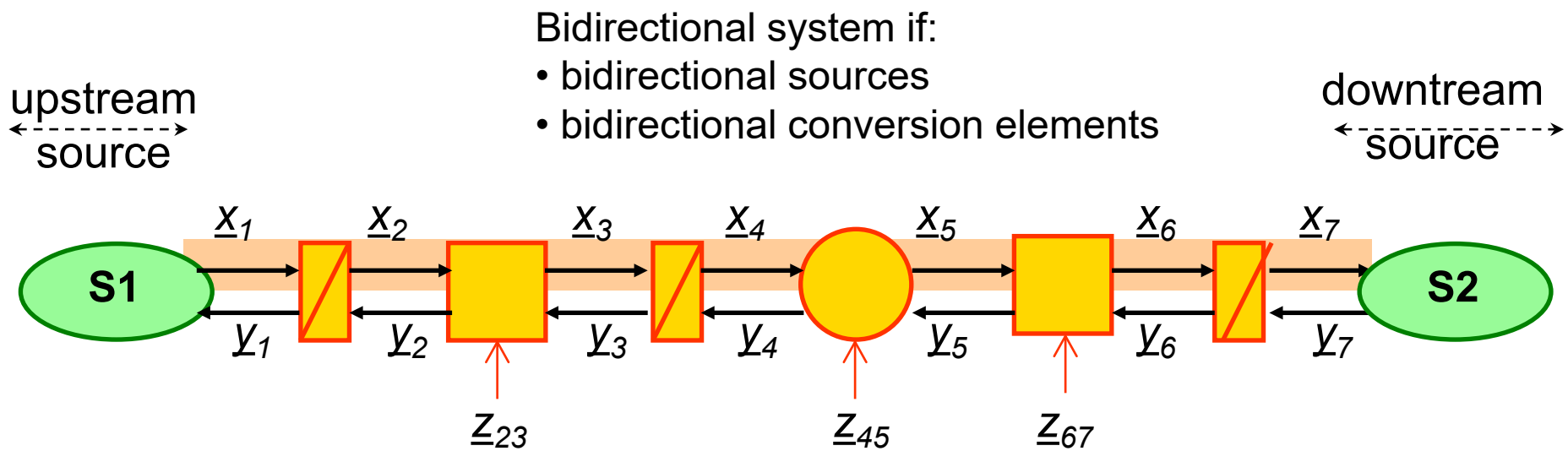
[Chen 2008]



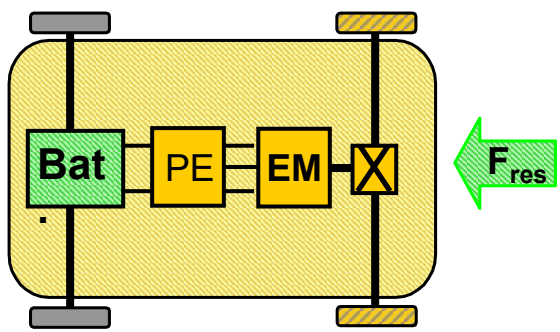
upstream source

downstream source

Convention: direction of positive power flow
(could be negative for bidirectional system)



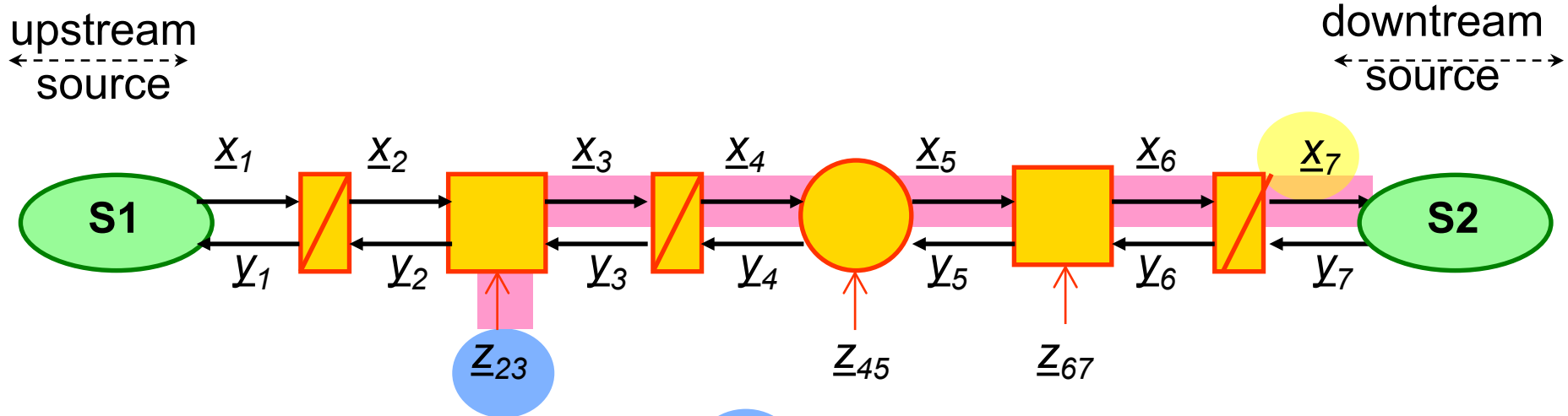
$P > 0$ action path: $X_1 \rightarrow X_2 \rightarrow X_3 \rightarrow X_4 \rightarrow X_5 \rightarrow X_6 \rightarrow X_7$
(e.g. acceleration) reaction path: $Y_1 \leftarrow Y_2 \leftarrow \dots \leftarrow Y_7$



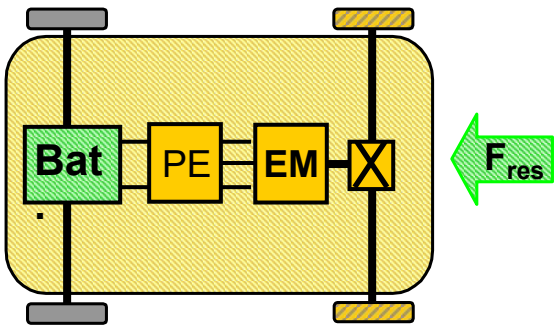
$P < 0$ action path: $Y_1 \leftarrow Y_2 \leftarrow \dots \leftarrow Y_7$
(e.g. braking) reaction path: $X_1 \rightarrow X_2 \rightarrow \dots \rightarrow X_7$

I/O independent of power flow direction
action/reaction dependent of power flow direction

Tuning path: causal path from the selected tuning input to the output to be controlled



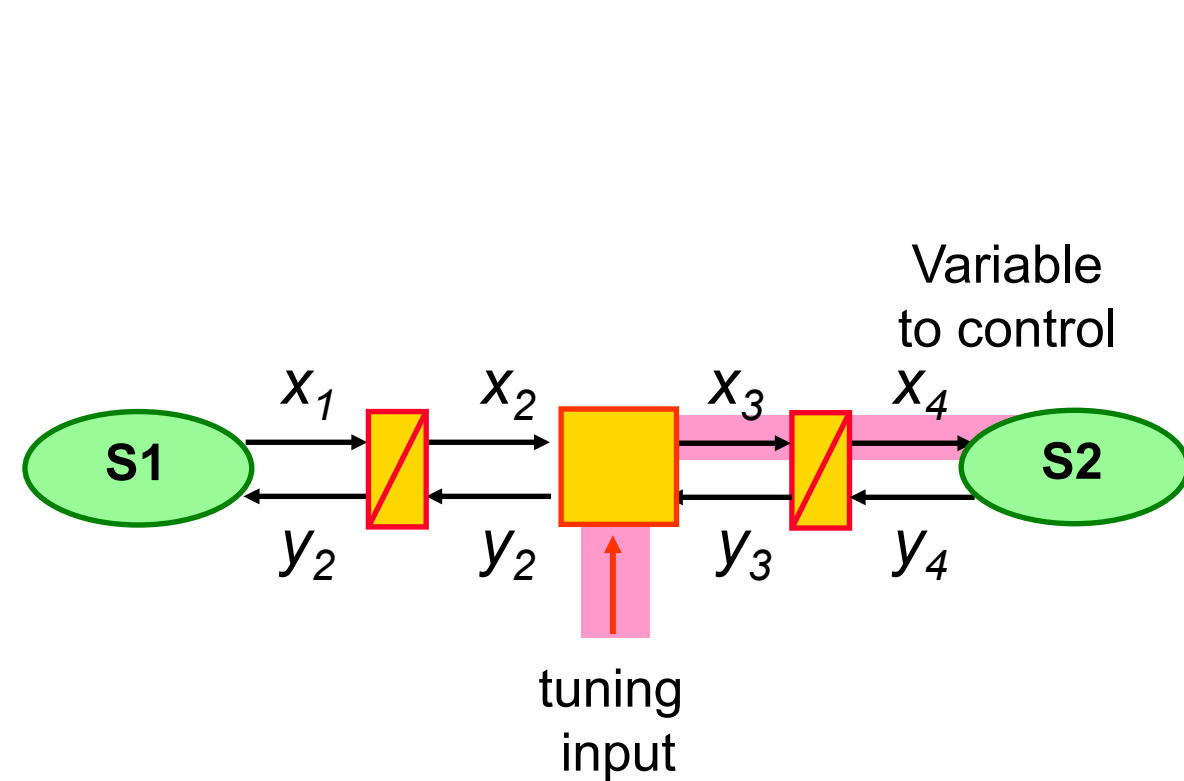
Technical requirements: action on z_{23} (e.g. converter modulation ratio) and x_7 (e.g. vehicle velocity) to be controlled



Tuning path: $z_{23} \rightarrow x_3 \rightarrow x_4 \rightarrow x_5 \rightarrow x_6 \rightarrow x_7$

The tuning path is **independent of the power flow direction**

(e.g. velocity control in acceleration AND regenerative braking)

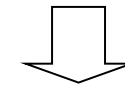


EMR = tool for analysis before control development

I/Os are independent of power flows

tuning paths:

- defined by the technical requirements
- independent of the power flow direction



EMR is adapted for control organization

unique control scheme whatever the power flow direction (e.g. traction or generator mode)

1

EMR elements

2

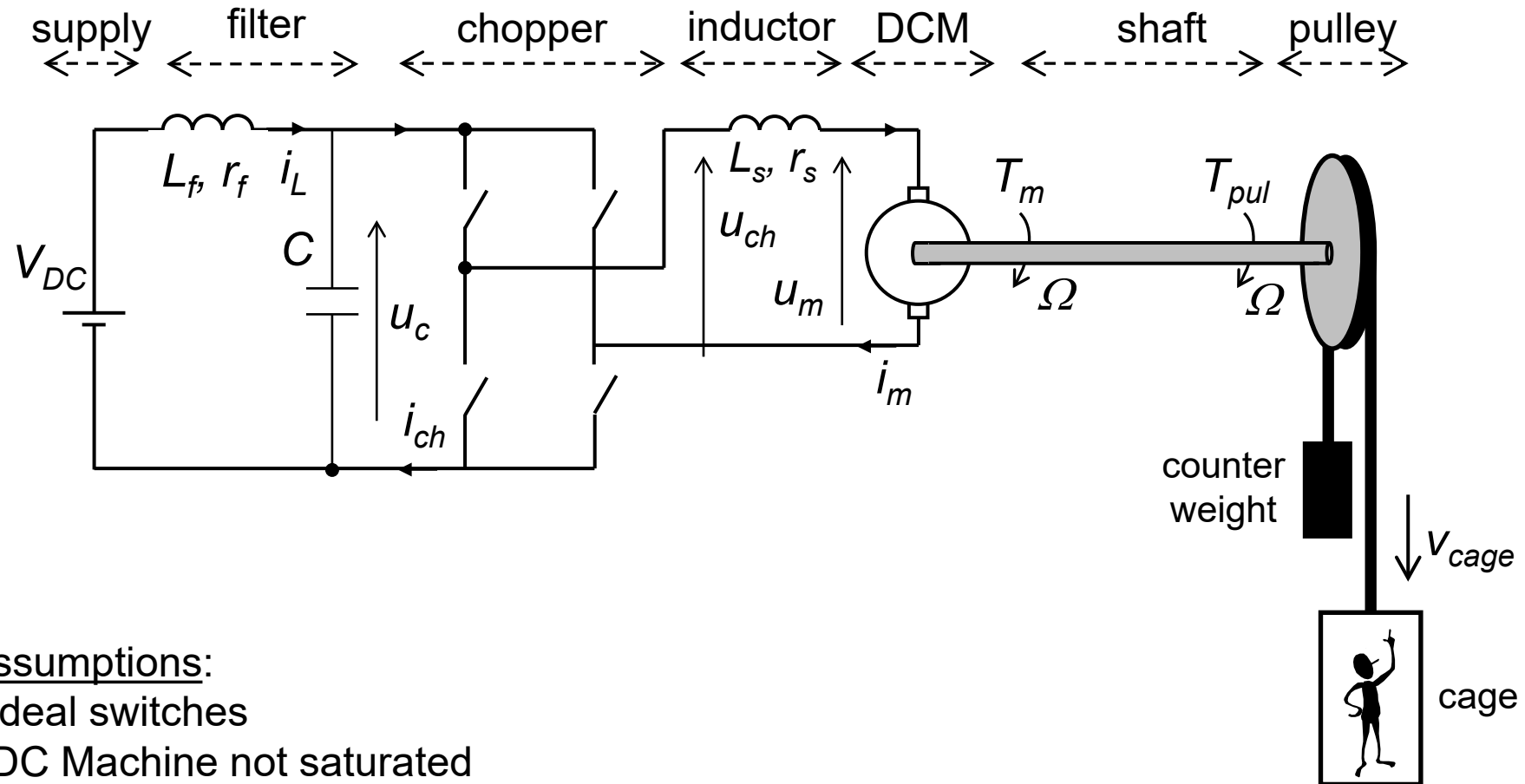
Association rules

3

EMR of a complete system

4

Example

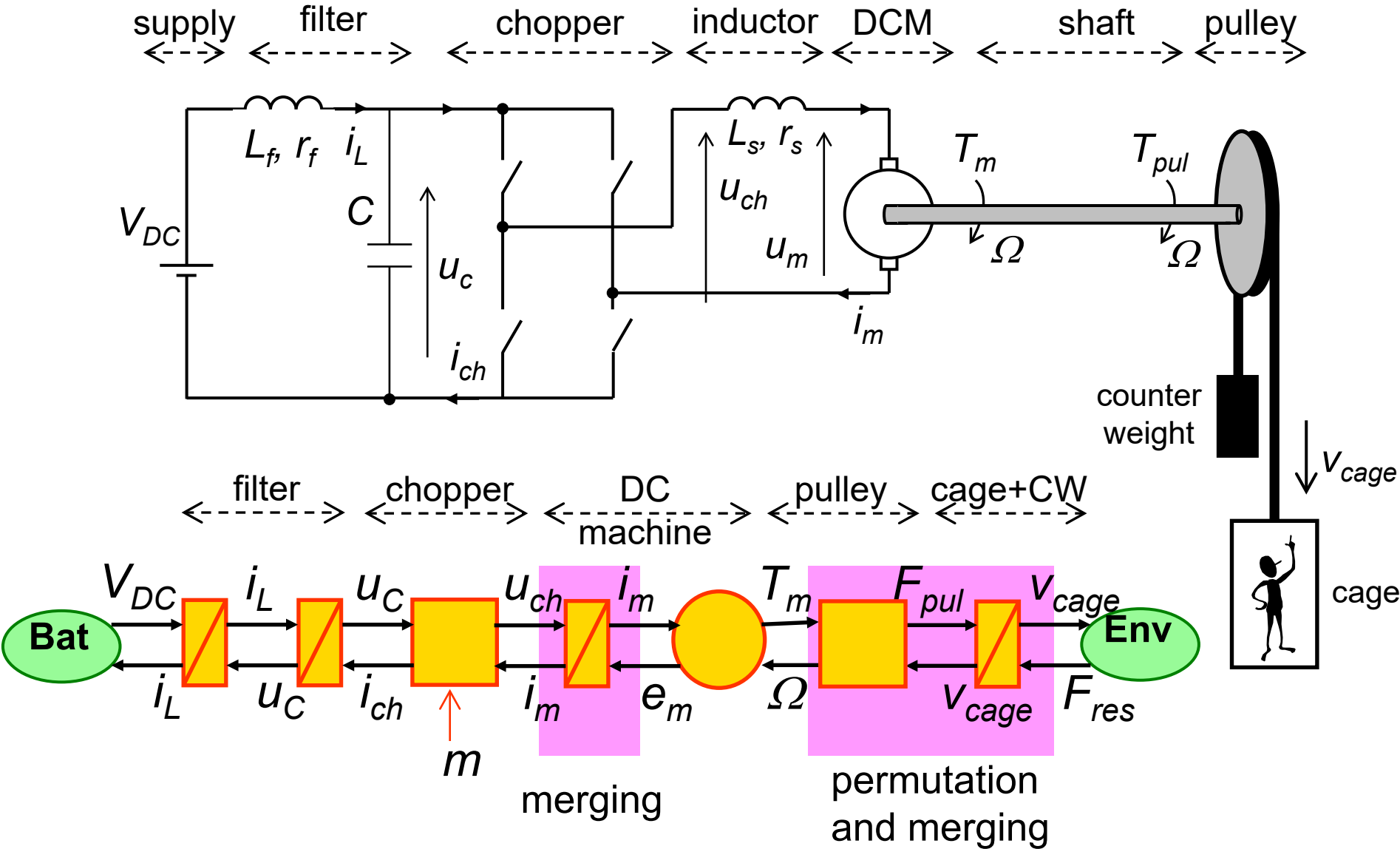


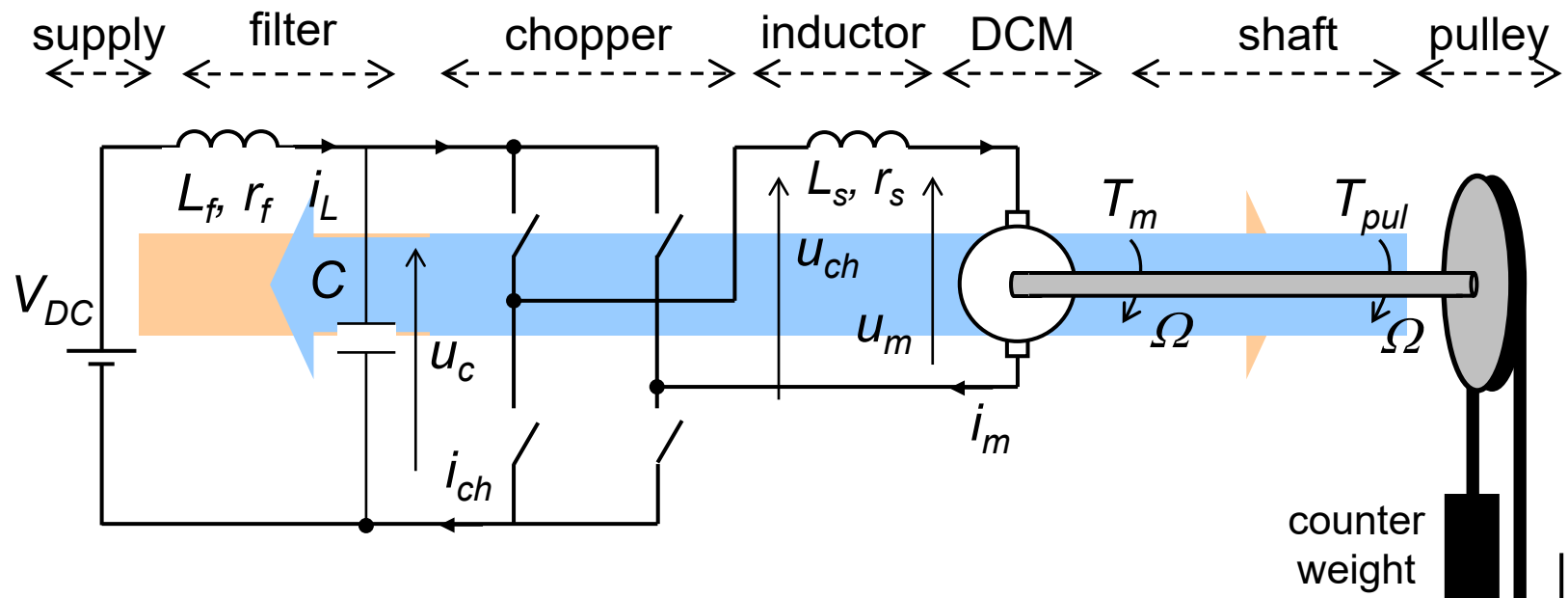
Assumptions:

- ideal switches
- DC Machine not saturated

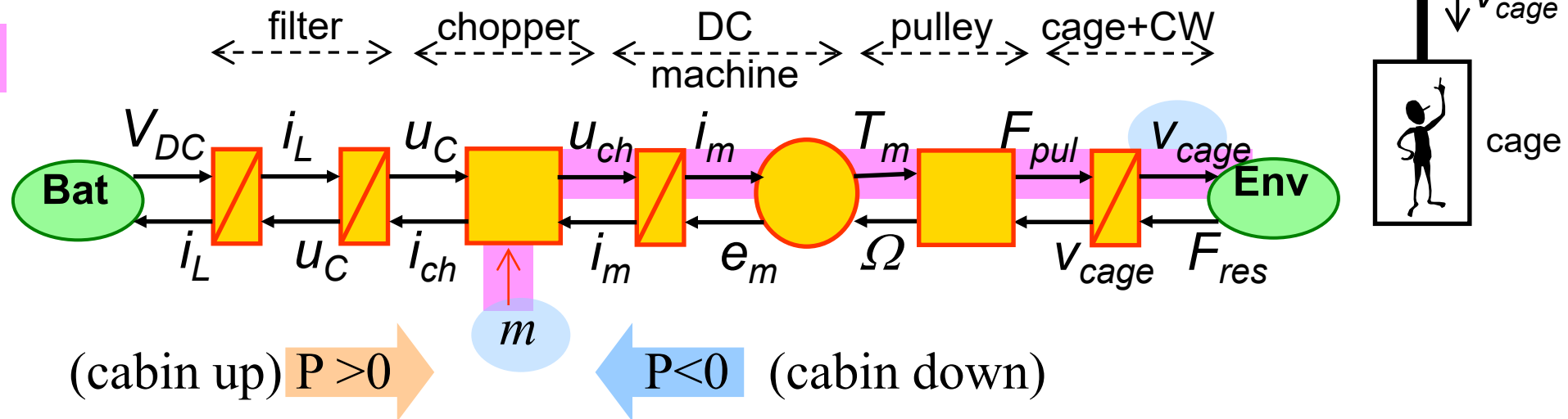
Technical requirement:

- control of velocity v_{cage}
- tuning input = modulation ratio of chopper m





tuning path





Conclusion



EMR = multi-physical graphical description

based on the interaction principle (systemic)
and the causality principle (energy)

Basic elements = energetic function

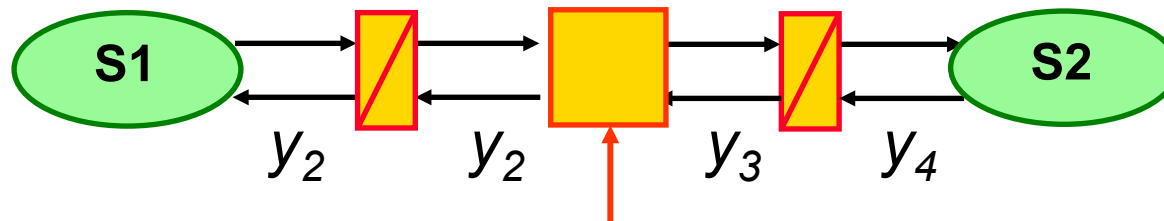
sources, accumulation, conversion and distribution of energy

Association rules = holistic property of systemic

enable keeping physical causality in conflict of association

Applications of EMR

analysis, simulation, control organization...



- [Bouscayrol 2000] A. Bouscayrol, & al. "Multimachine Multiconverter System: application for electromechanical drives", *European Physics Journal - Applied Physics*, vol. 10, no. 2, May 2000, pp. 131-147 (common paper GREEN Nancy, L2EP Lille and LEEI Toulouse, according to the SMM project of the GDR-SDSE).
- [Bouscayrol 2012] A. Bouscayrol, J. P. Hautier, B. Lemaire-Semail, "Graphic Formalisms for the Control of Multi-Physical Energetic Systems", *Systemic Design Methodologies for Electrical Energy*, tome 1, Analysis, Synthesis and Management, Chapter 3, ISTE Willey editions, October 2012, ISBN: 9781848213883
- [Bouscayrol 2023] A. Bouscayrol, B. Lemaire-Semail, "Energetic Macroscopic Representation and Inversion-Based Control", Encyclopedia of electrical and electronic power engineering, Vol. 3, pp 365-375, Elsevier, DOI : 10.1016/B978-0-12-821204-2.00117-3, ISBN : 978-0-12-823211-8, 2023.**
- [Chen 2008] K. Chen, A. Bouscayrol, W. Lhomme, "Energetic Macroscopic Representation and Inversion-based control: Application to an Electric Vehicle with an electrical differential", *Journal of Asian Electric Vehicles*, Vol. 6, no.1, June issue, 2008, pp. 1097-1102.
- [Lhomme 2014] W. Lhomme, P. Delarue, A. Bouscayrol, P. Barrade, "La REM, formalismes multiphysique de commande des systèmes énergétiques", *Les Techniques de l'Ingénieur*, Référence D3066, Novembre 2014 (text in French, lift example)



Thanks for your attention!

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