

« EMR AND INVERSION-BASED CONTROL OF AN ELECTRIC VEHICLE »

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Studied EV

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EMR of the studied EV

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Inversion-based control of the EV



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1. Studied EV

- Simplified description of a Renault Zoe -

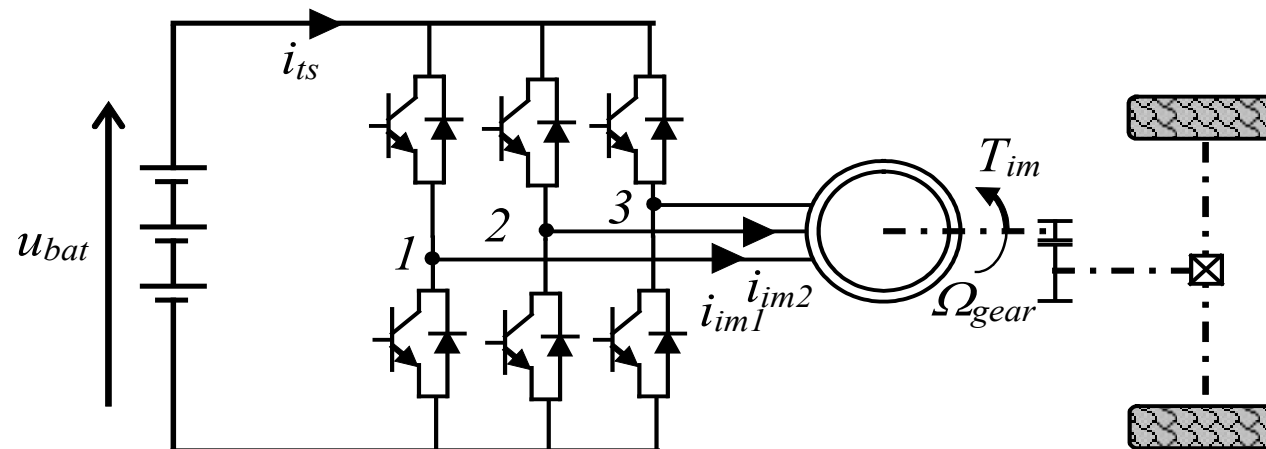
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Renault Zoe main characteristics (2018)

- 80kW – 100kW Synchronous Motor
- 41Ah Li NMC battery
- 1555 kg (empty mass)

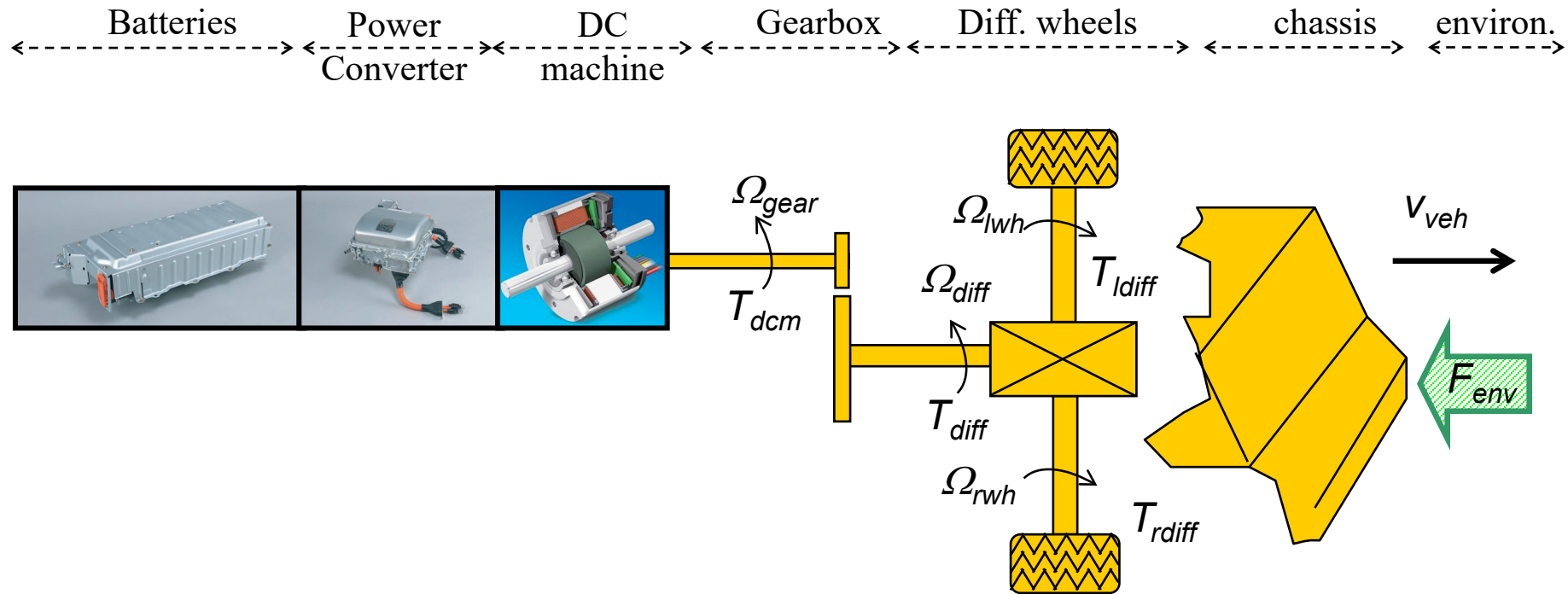


Objective:

- Illustration of EMR-IBC methodology: control of the traction system in straight lines
- Introduction to simulation session

Simplifications and assumptions for analysis and EMR

- A non-saturated permanent magnet DC machine is considered (instead of Synchronous machine)
- Ideal power converter (no losses)
- Inertia of rotating masses are not taken in account
- Contact wheel/ground with no slip and pneumatic deformation
- Mechanical brakes are not considered

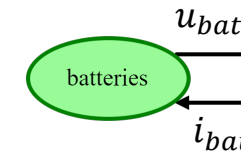
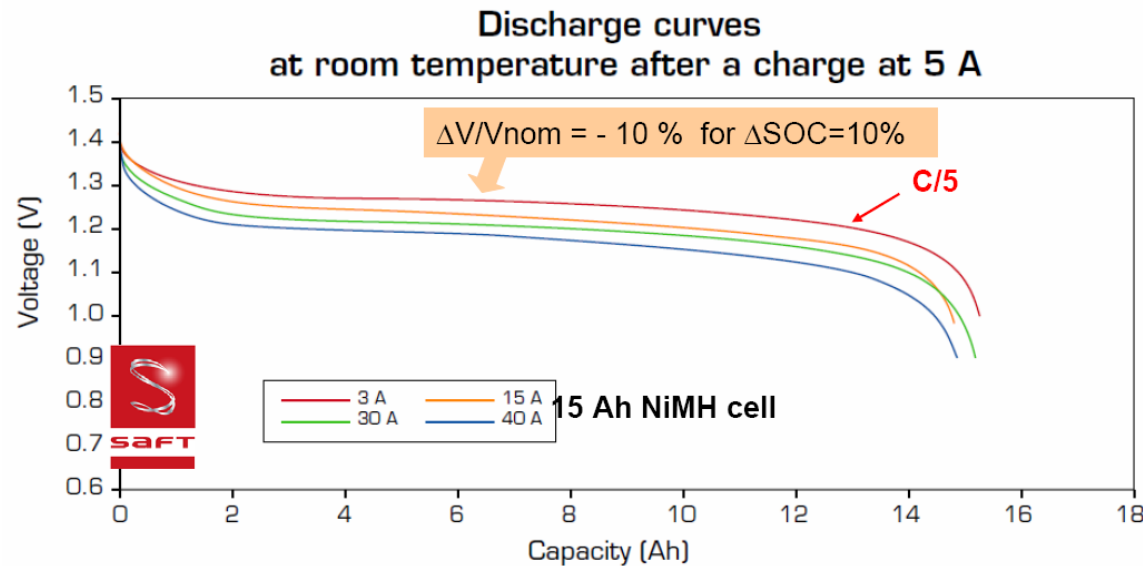
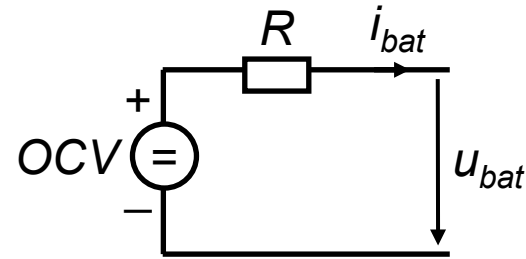




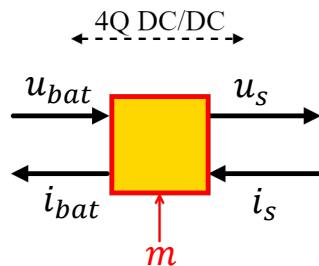
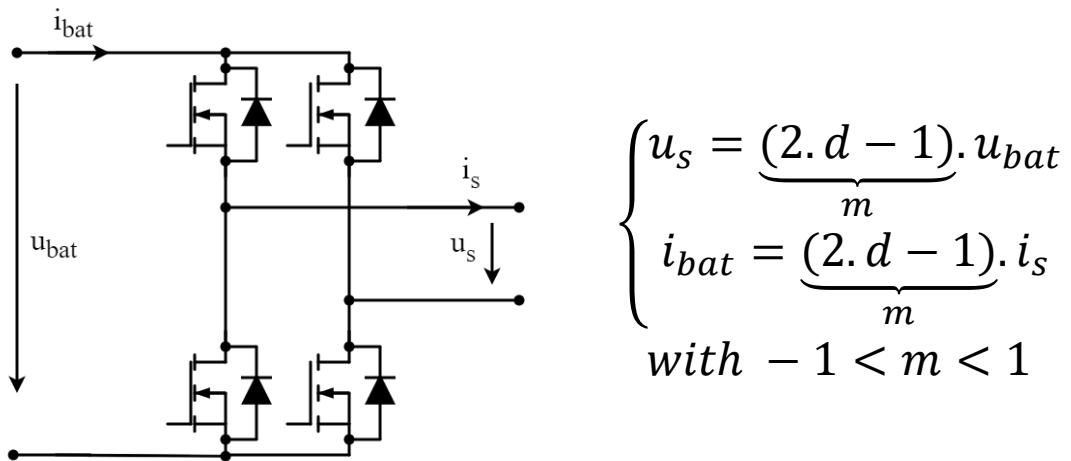
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EMR of the studied EV

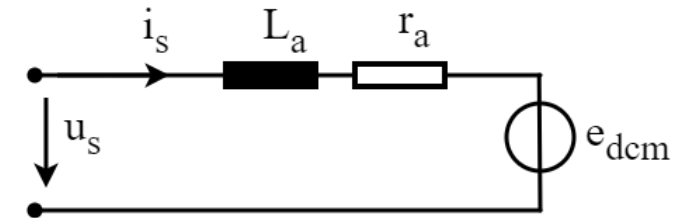
- Terminal element of system – Environnement of system
 - Must be modelled anyway
 - Open Circuit Voltage (OCV)
 - Internal impedance (R):
 - State of Charge (SOC)



- 4Q DC/DC converter for full reversibility
 - Introducing d as the main duty cycle
 - Definition of an average model ($0 < d < 1$)

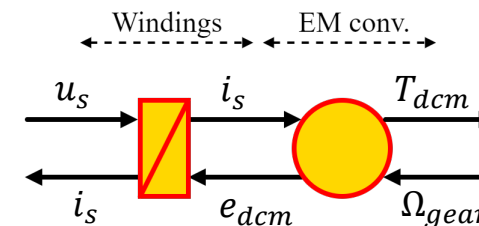


- DC machine with permanent magnets
 - Electrical equations

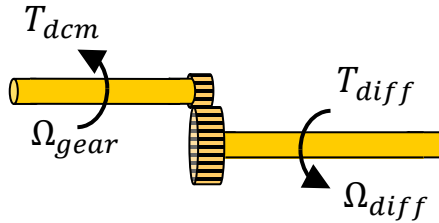


- Electro-mechanical conversion

$$\begin{cases} T_{dcm} = k_{dcm} \cdot i_s \\ e_{dcm} = k_{dcm} \cdot \Omega_{gear} \end{cases}$$



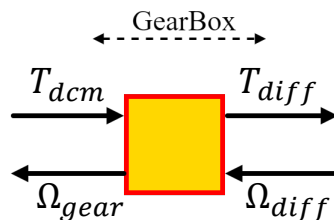
• Gearbox



- k_{gear} : transformation ratio
- η_{gear} : efficiency, p : correction exponent

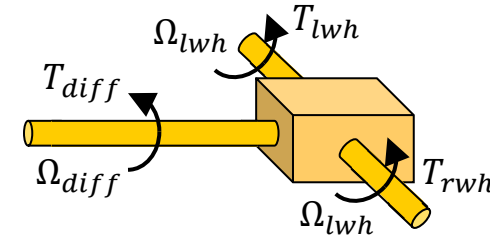
$$\begin{cases} T_{diff} = \eta_{gear}^p k_{gear} T_{dcm} \\ \Omega_{gear} = k_{gear} \Omega_{diff} \end{cases}$$

with $\begin{cases} p = 1 & \text{if } \Omega_{diff} T_{diff} \geq 0 \\ p = -1 & \text{if } \Omega_{diff} T_{diff} < 0 \end{cases}$



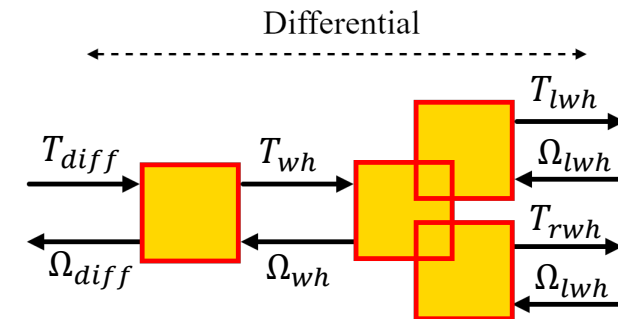
• Differential

- 2 functions in 1

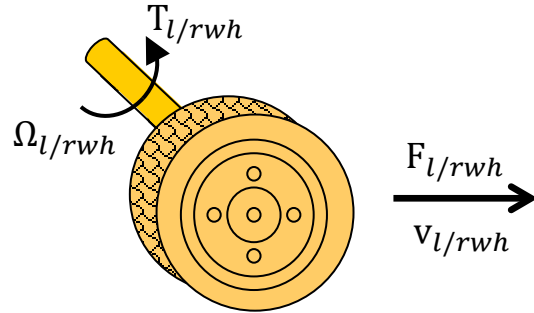


- k_{diff} : transformation ratio
- η_{diff} : efficiency, p : correction exponent

$$\begin{cases} T_{wh} = \eta_{diff}^p k_{diff} T_{diff} \\ \Omega_{diff} = k_{diff} \Omega_{wh} \end{cases} \text{ and } \begin{cases} T_{ldiff} = T_{rdiff} = \frac{1}{2} T_{wh} \\ \Omega_{wh} = \frac{1}{2} (\Omega_{lwh} + \Omega_{rwh}) \end{cases}$$

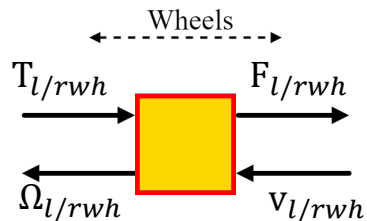


• Wheels



– R_{wh} : wheels radius

$$\begin{cases} F_{l/rwh} = k_{wh} \cdot T_{l/rwh} \\ \Omega_{l/rwh} = k_{whf} \cdot v_{l/rwh} \end{cases} \quad \text{with} \quad k_{wh} = \frac{1}{R_{wh}}$$

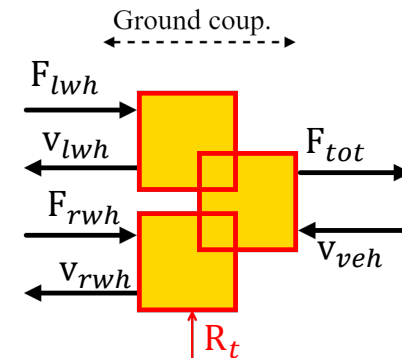
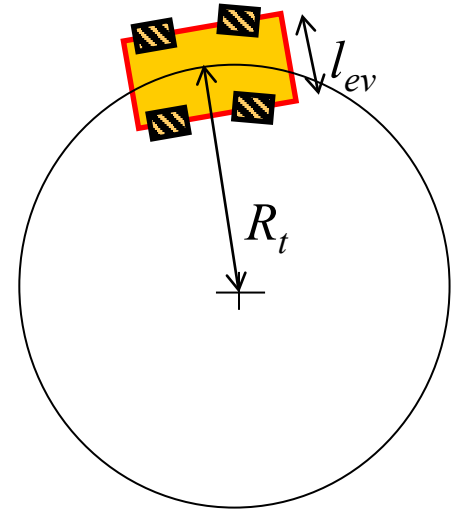


• Ground coupling

– R_t : turning radius

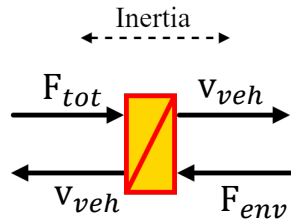
– L_{ev} : vehicle width

$$\begin{cases} v_{lwh} = \left(1 + \frac{1}{2} \cdot \frac{l_{ev}}{R_t}\right) \cdot v_{veh} \\ v_{rwh} = \left(1 - \frac{1}{2} \cdot \frac{l_{ev}}{R_t}\right) \cdot v_{veh} \\ F_{tot} = F_{lwh} + F_{rwh} \end{cases}$$



- Inertia (Chassis)
 - M_{veh} : total mass of the vehicle

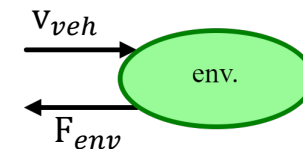
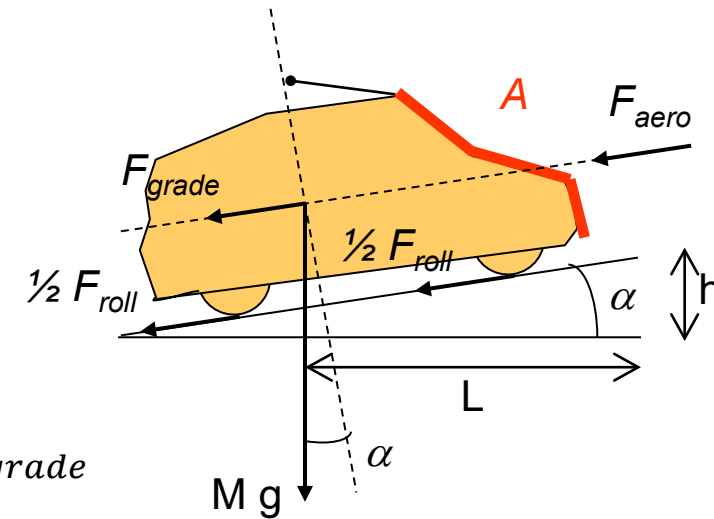
$$M_{veh} \cdot \frac{dv_{veh}}{dt} = F_{tot} - F_{env}$$



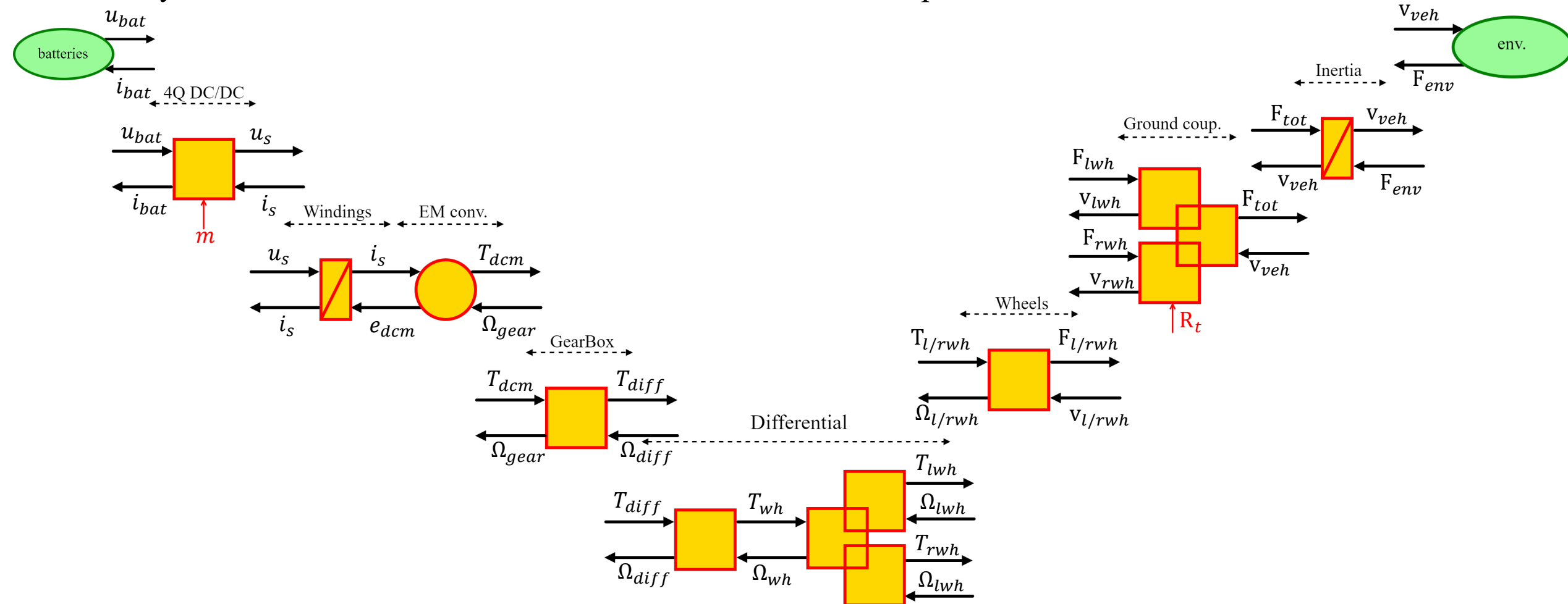
- Environment - Terminal element of system – Must be modelled anyway
 - F_{aero} : aerodynamic resistance
 - F_{roll} : rolling resistance
 - F_{grade} : grade resistance

$$\begin{cases} F_{aero} = \frac{1}{2} \rho_{air} \cdot A \cdot C_x \cdot v_{veh}^2 \\ F_{roll} = k_{roll} \cdot M_{veh} \cdot g \cdot \cos \alpha \\ F_{grade} = M_{veh} \cdot g \cdot \sin \alpha \end{cases}$$

$$F_{env} = F_{aero} + F_{roll} + F_{grade}$$



- All subsystems have been modelled and represented
 - They can be associated as far as: IOs for one element are compatible with IOs of the consecutive elements

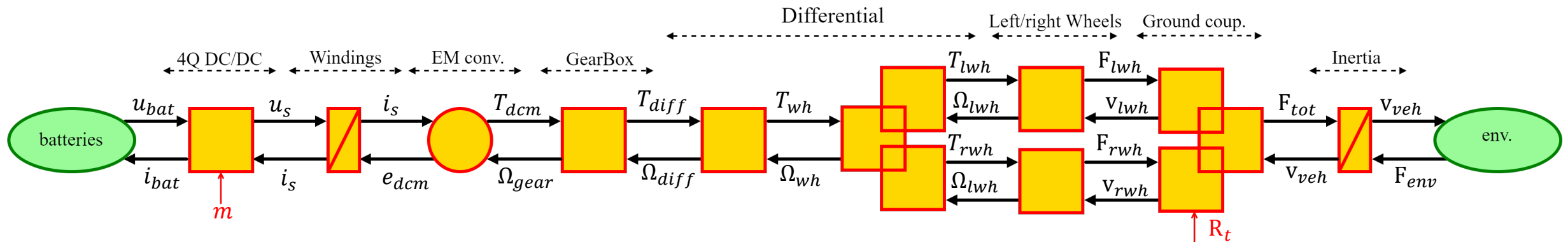
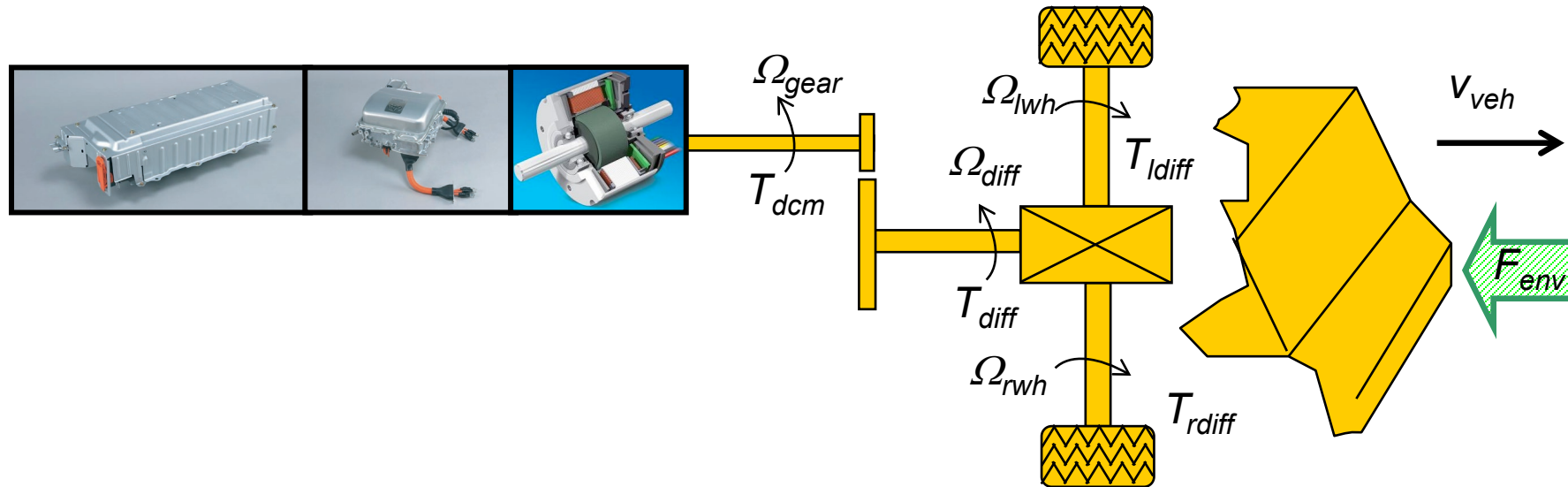
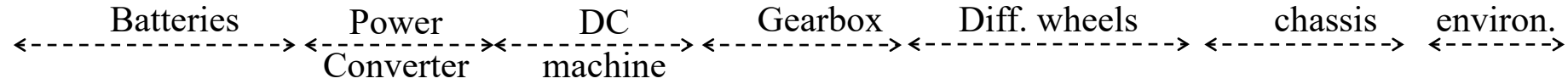


EMR and control of an EV

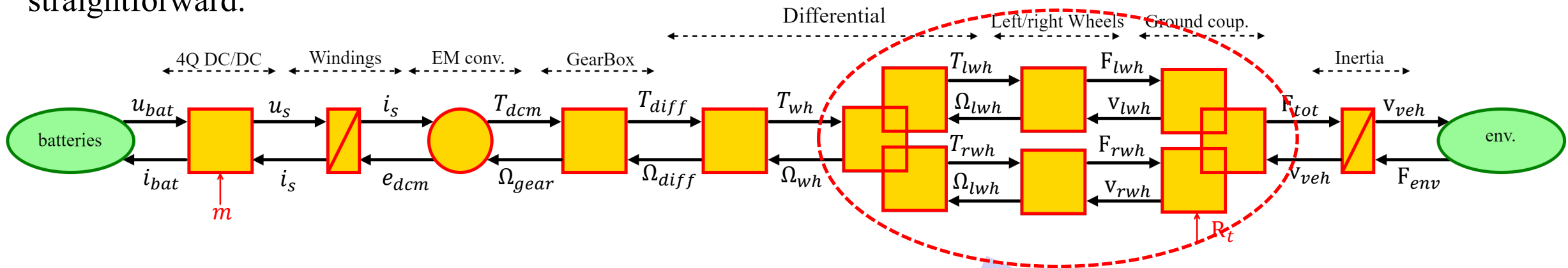
- Structural vs. Functional representation -

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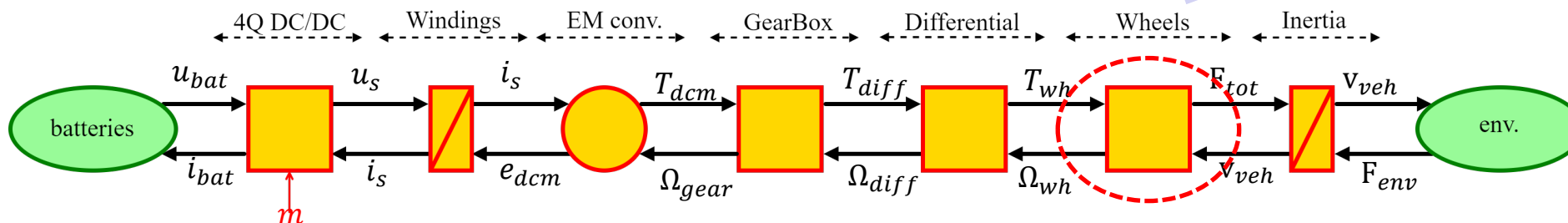


- Simplifications under conditions: Contact wheel/ground with no slip and pneumatic deformation, the vehicle goes straightforward.



If the vehicle drives in a straight line ($R_t = \infty$), an equivalent wheel is sufficient

model reduction



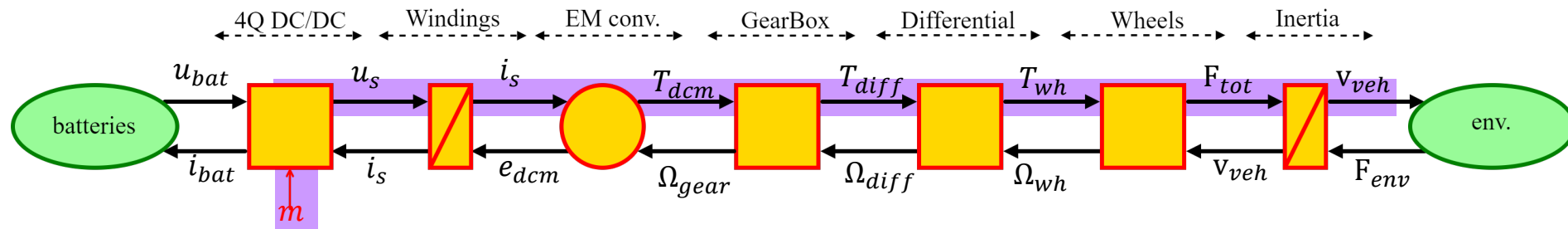
$$\begin{cases} F_{tot} = \frac{1}{R_{wh}} T_{wh} \\ \Omega_{wh} = \frac{1}{R_{wh}} v_{veh} \end{cases}$$



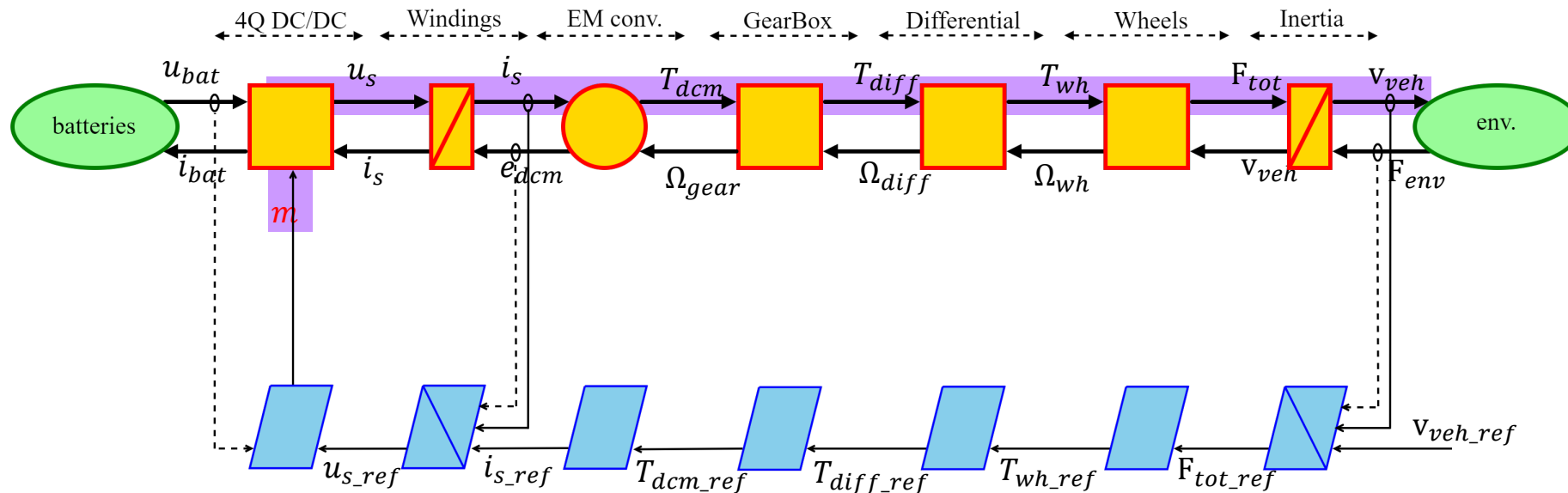
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Inversion-based control of the studied EV

- Objectives: control of vehicle speed
- Constraints: DC machine current limitation (Torque limitation)
- Tuning variable: modulation function of the 4Q converter
 - Tuning path: from the tuning variable to the objective through constraints



- Inversion of the EMR's éléments, from the objectif to the tuning parameter



Maximum Control Structure:

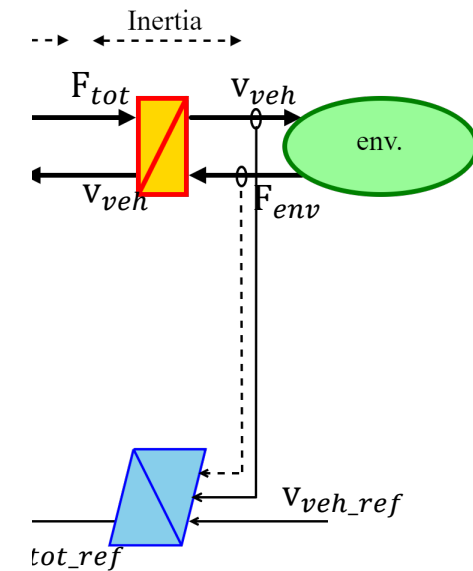
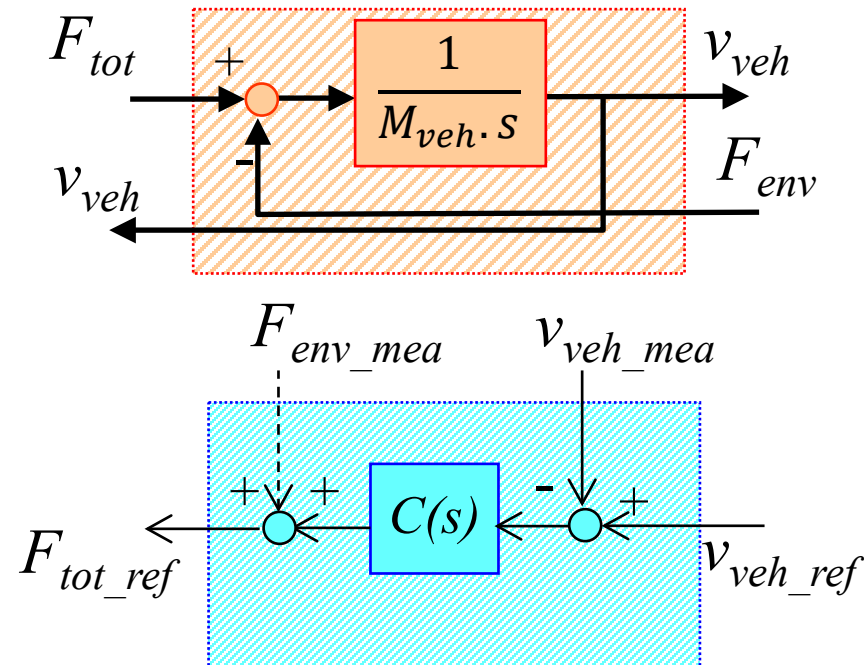
- inversion of each element step-by-step
- all variables are supposed to be measurable

- Direct inversion vs. Undirect inversion -

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- Undirect inversion: controller for the inversion of accumulation elements

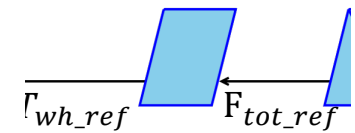
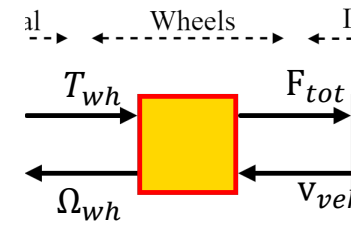
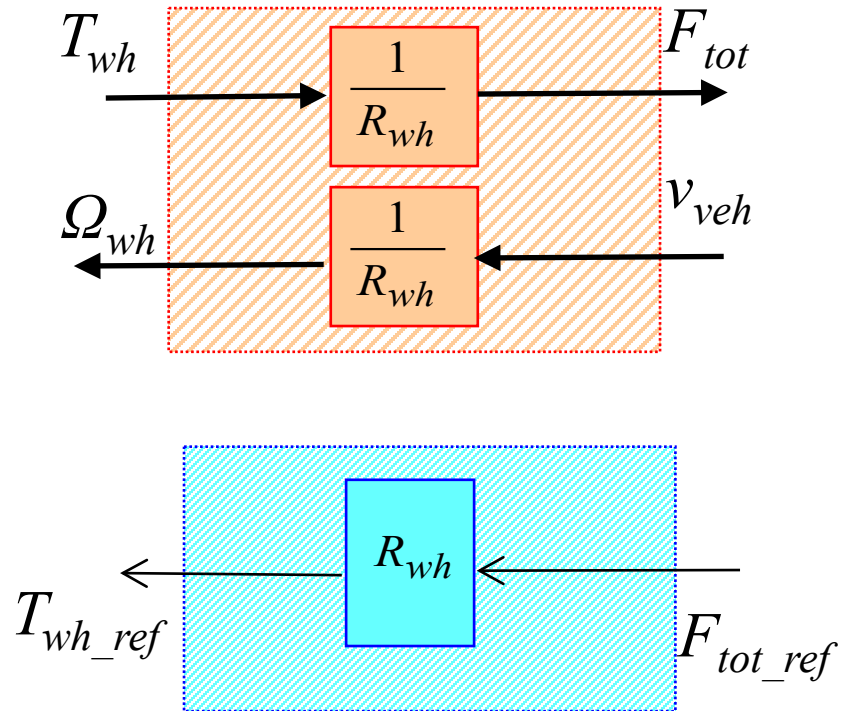


- Direct inversion vs. Undirect inversion -

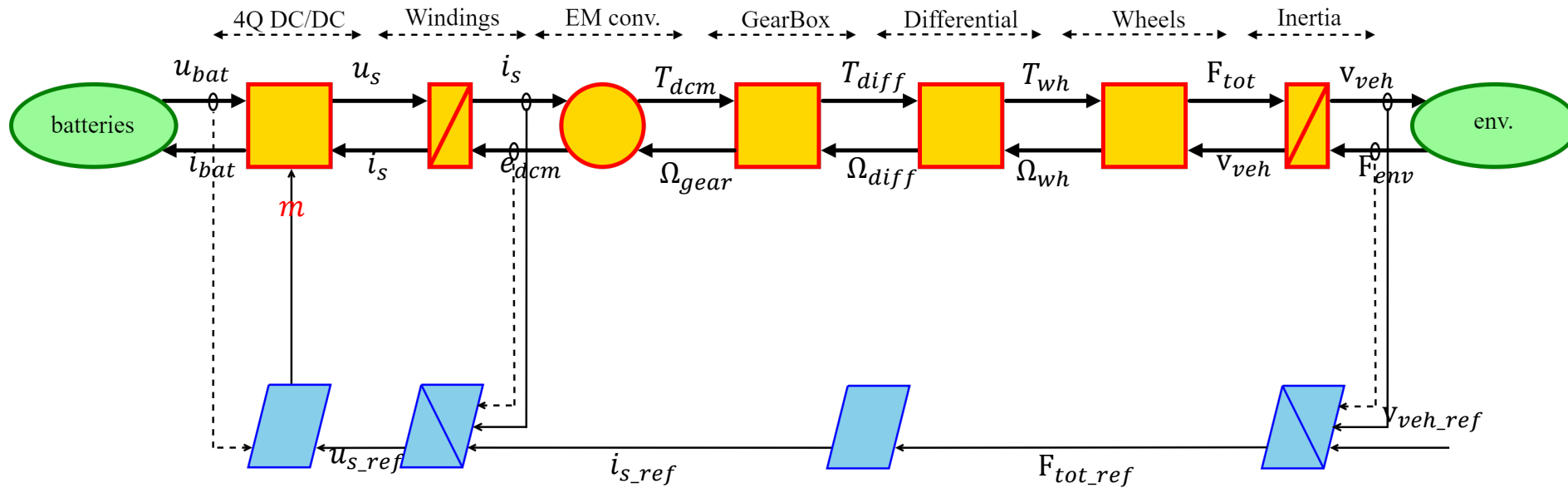
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- Direct inversion: pure model inversion

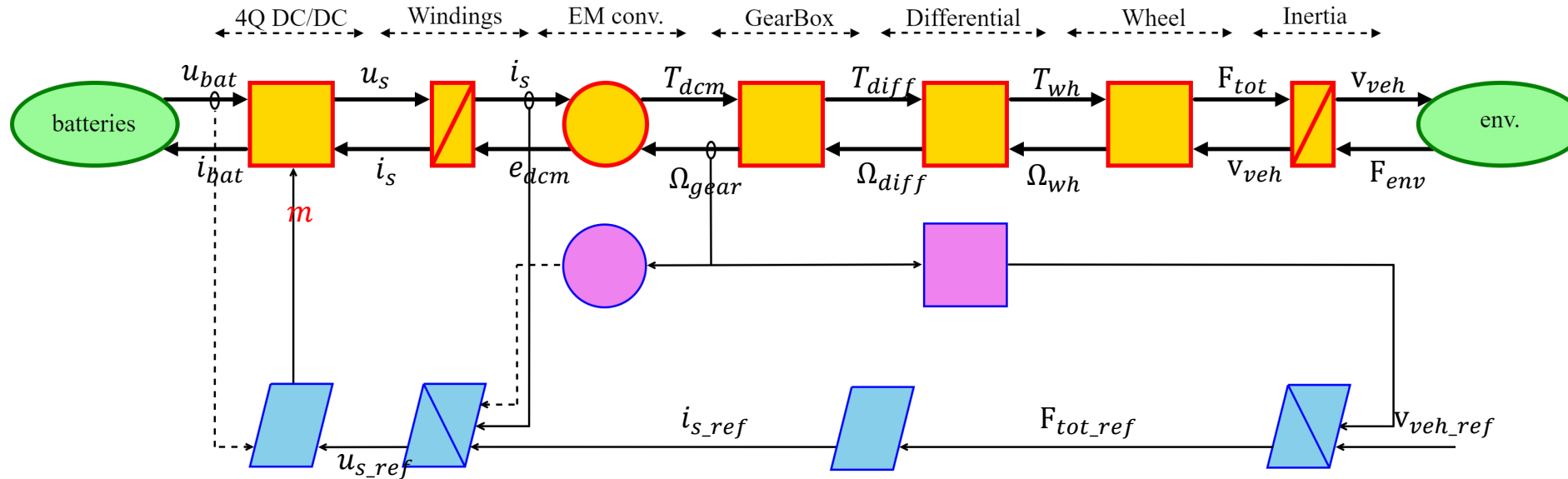


- Merge of all «Direct Inversion» elements that are series connected



$$F_{tot} = \underbrace{K_{dcm} \cdot K_{gear} \cdot K_{diff} \cdot K_{wh}}_K \cdot i_s \Rightarrow i_{s_ref} = \frac{1}{\underbrace{K_{dcm} \cdot K_{gear} \cdot K_{diff} \cdot K_{wh}}_{1/K}} \cdot F_{tot_ref}$$

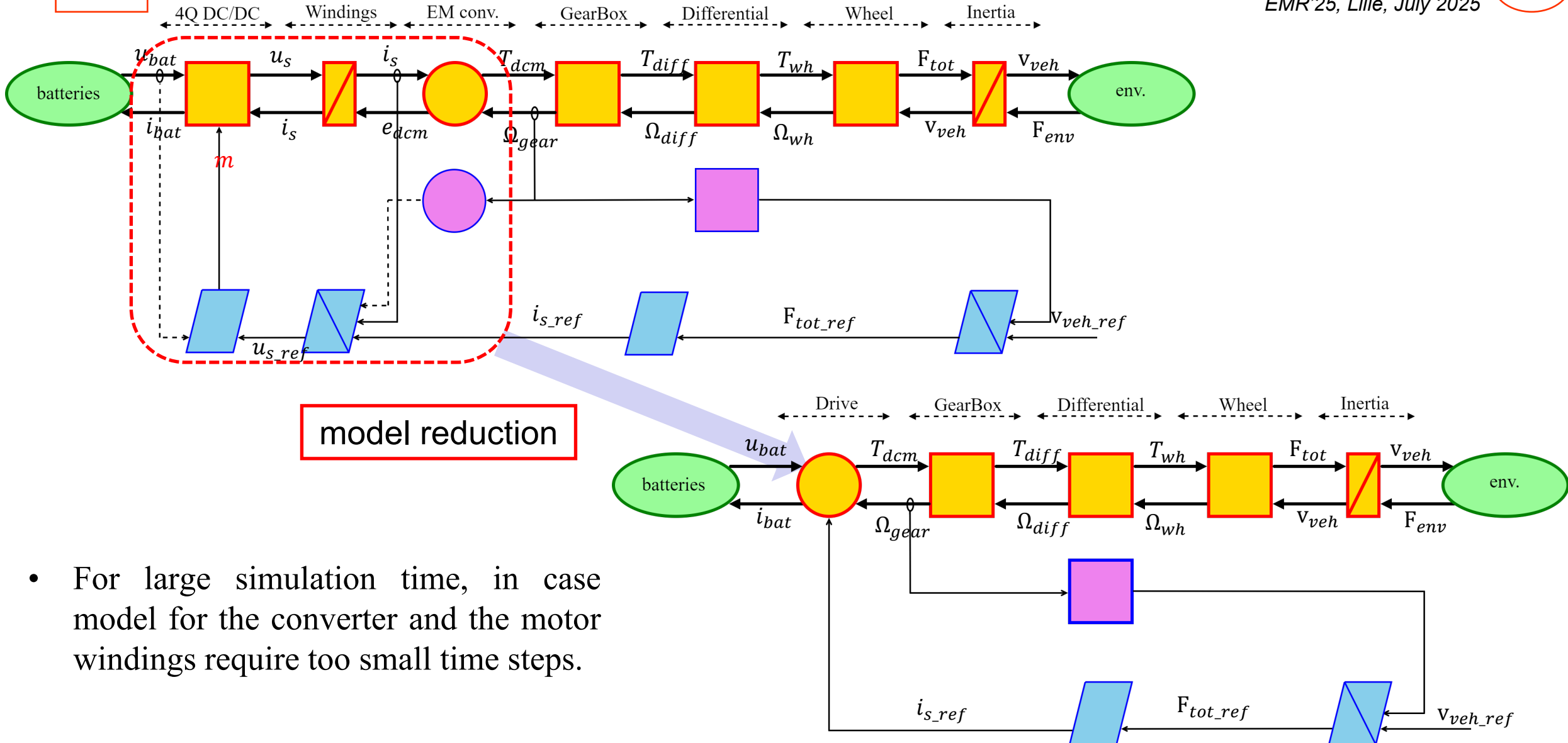
- Check if all measures can be implemented
- For measures that are not physically accessible, check if models behind EMR symbol can be used for estimation,



- Model simplification -

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Conclusion

- ❖ EMR: powerful approach for describing and representing complex and multiphysic systems
- ❖ IBC: based on inversion rules, allow a safe design for control design
- ❖ Case considered in this contribution is based on DC motors, Anyway, such an approach is obviously applicable with benefits to more modern technologies:
 - Induction motor(s)
 - PM synchronous motor(s)
 - etc.
- ❖ EMR for EVs:
 - In the 1st step: Simplified model using DC motor with chopper
(for IM, PMSM: the same principles are applied)
 - EMR: identification of functions linked to sub-systems,
 - Inversion-based control, from inversion of EMR functions
 - First step for Simulation implementation: in Matlab/Simulink using EMR library (for example)



Prof. Philippe Barrade, University of Applied Sciences Western Switzerland, Institute for Systems Engineering. Ph.D. in Electrical Engineering at Institut National Polytechnique de Toulouse (1997)
Research topics: Power Electronics, Real-time Control, Modelling, Real-time simulation and system design.

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Coordinator of the CUMIN interdisciplinary programme
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PhD in Electrical Engineering at University of Toulouse (1995)
Research topics: EMR formalism, HIL testing, control & EV-HEVs

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- [Bouscayrol 2012] A. Bouscayrol, J. P. Hautier, B. Lemaire-Semail, "Graphic Formalisms for the Control of Multi-Physical Energetic Systems", Systemic Design Methodologies for Electrical Energy, tome 1, Analysis, Synthesis and Management, Chapter 3, ISTE Willey editions, October 2012, ISBN: 9781848213883
- [Bouscayrol 2015] A. Bouscayrol, Philippe Delarue, Walter Lhomme, Betty Lemaire-Semail, "Teaching drive control using Energetic Macroscopic Representation – From maximal to practical control schemes", EPE'15 ECCE Europe, Geneva (Switzerland), September 2015.
- [Bouscayrol 2023] A. Bouscayrol, B. Lemaire-Semail, "Energetic Macroscopic Representation and Inversion-Based Control ", Encyclopedia of electrical and electronic power engineering, Vol. 3, pp 365-375, Elsevier, DOI : 10.1016/B978-0-12-821204-2.00117-3, ISBN : 978-0-12-823211-8, 2023
- [Nguyen 2020] C. T. P. Nguyen, J. P. F. Trovao, B. -H. Nguyen and M. C. Ta, "Powertrain Analysis of an All-Wheel-Drive Off-Road Electric Vehicle," 2019 IEEE Vehicle Power and Propulsion Conference (VPPC), Hanoi, Vietnam, 2019, pp. 1-6, doi: 10.1109/VPPC46532.2019.8952550.
- [Nguyen 2019] B. -H. Nguyen, R. German, J. P. F. Trovão and A. Bouscayrol, "Real-Time Energy Management of Battery/Supercapacitor Electric Vehicles Based on an Adaptation of Pontryagin's Minimum Principle," in IEEE Transactions on Vehicular Technology, vol. 68, no. 1, pp. 203-212, Jan. 2019, doi: 10.1109/TVT.2018.2881057.